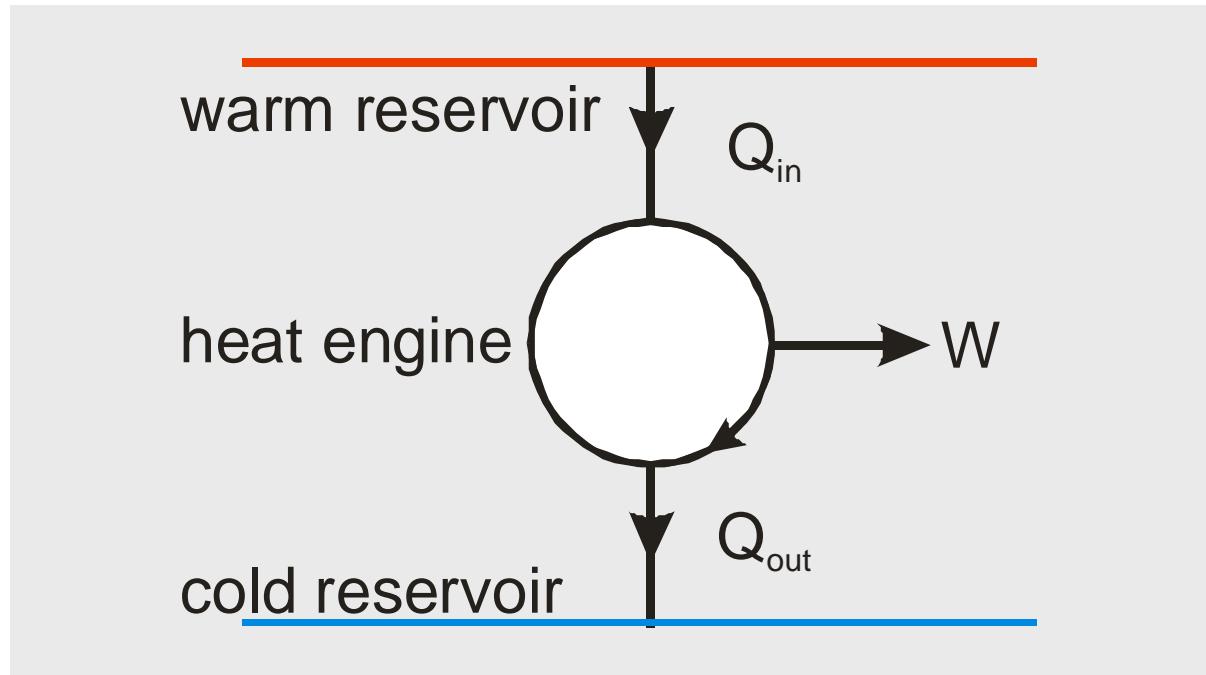


# Low Enthalpy Cycles - Power Plant Concepts



Silke Köhler<sup>1</sup>, Felix Ziegler<sup>2</sup>

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<sup>2</sup>*Technical University of Berlin (TUB)*

## Heat source

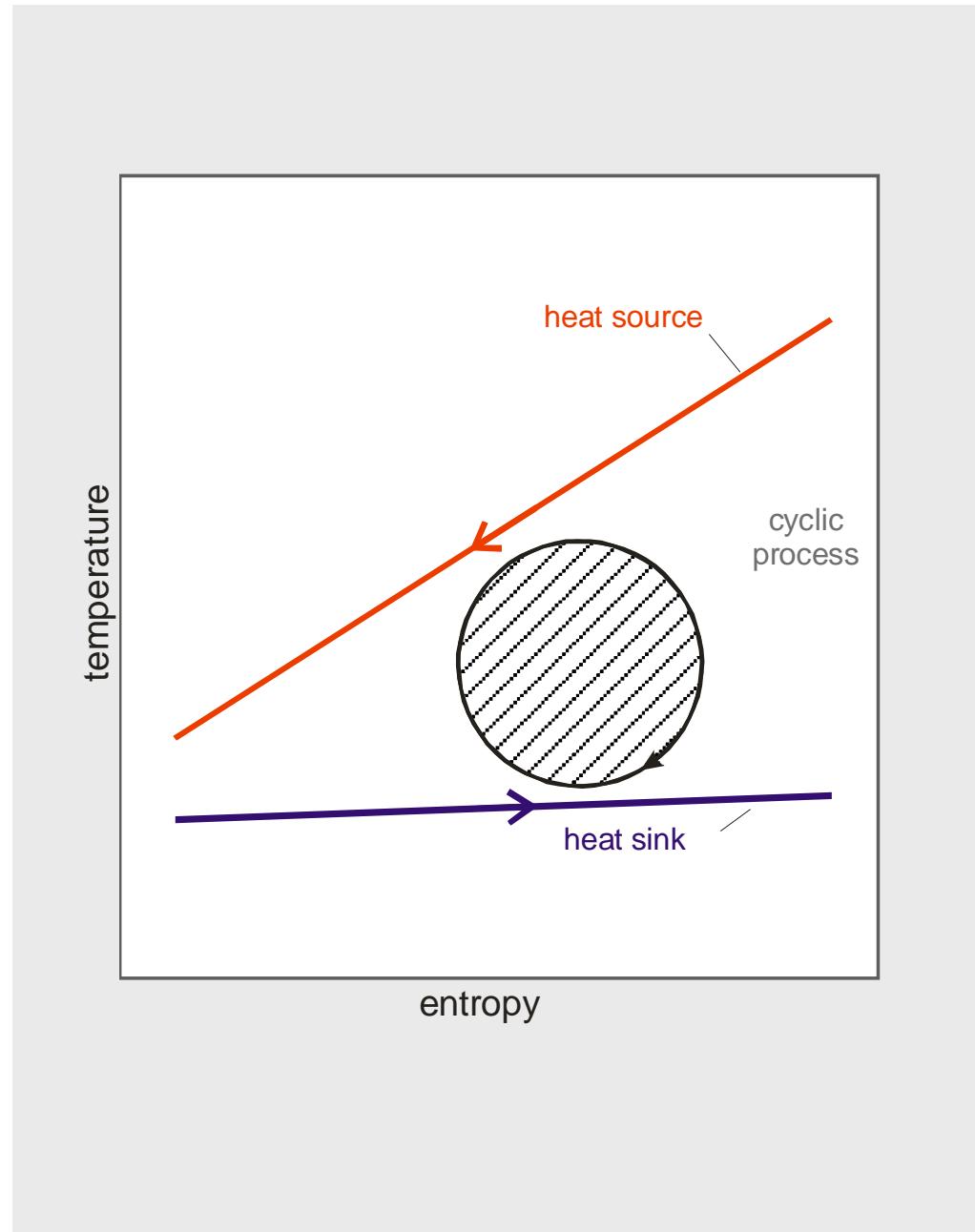
- Temperature  
 $100^{\circ}\text{C} - 200^{\circ}\text{C}$
- Mass flow rate  
 $50 - 200 \text{ m}^3/\text{h}$   
( $\sim 14 - 55 \text{ kg/s}$ )
- Limited heat capacity  
 $\sim 5$  to  $50 \text{ MW}_{\text{th}}$  per well
- Sensible heat

Goal: Electricity generation

## Tools

- Cycles and systems
- Design and optimisation

→ Suitability of different cycles  
for particular applications



Internally and externally reversible

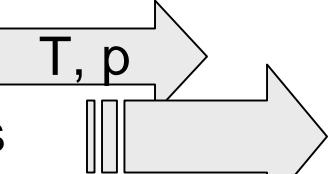
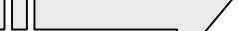
- Carnot Cycle
- Lorentz Cycle
- Triangular Cycle

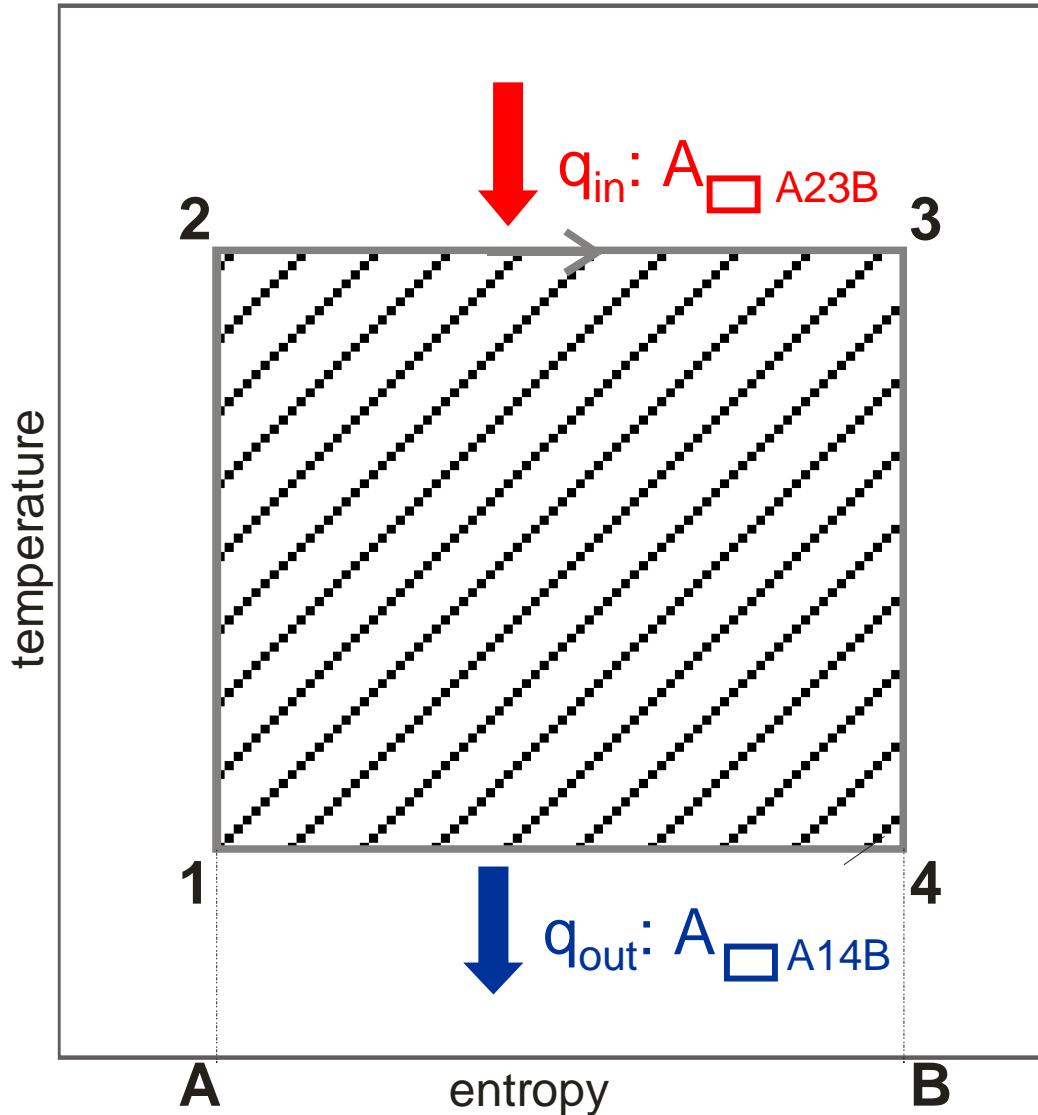
Internally reversible

- Rankine Cycle - ideal cycle for steam power processes

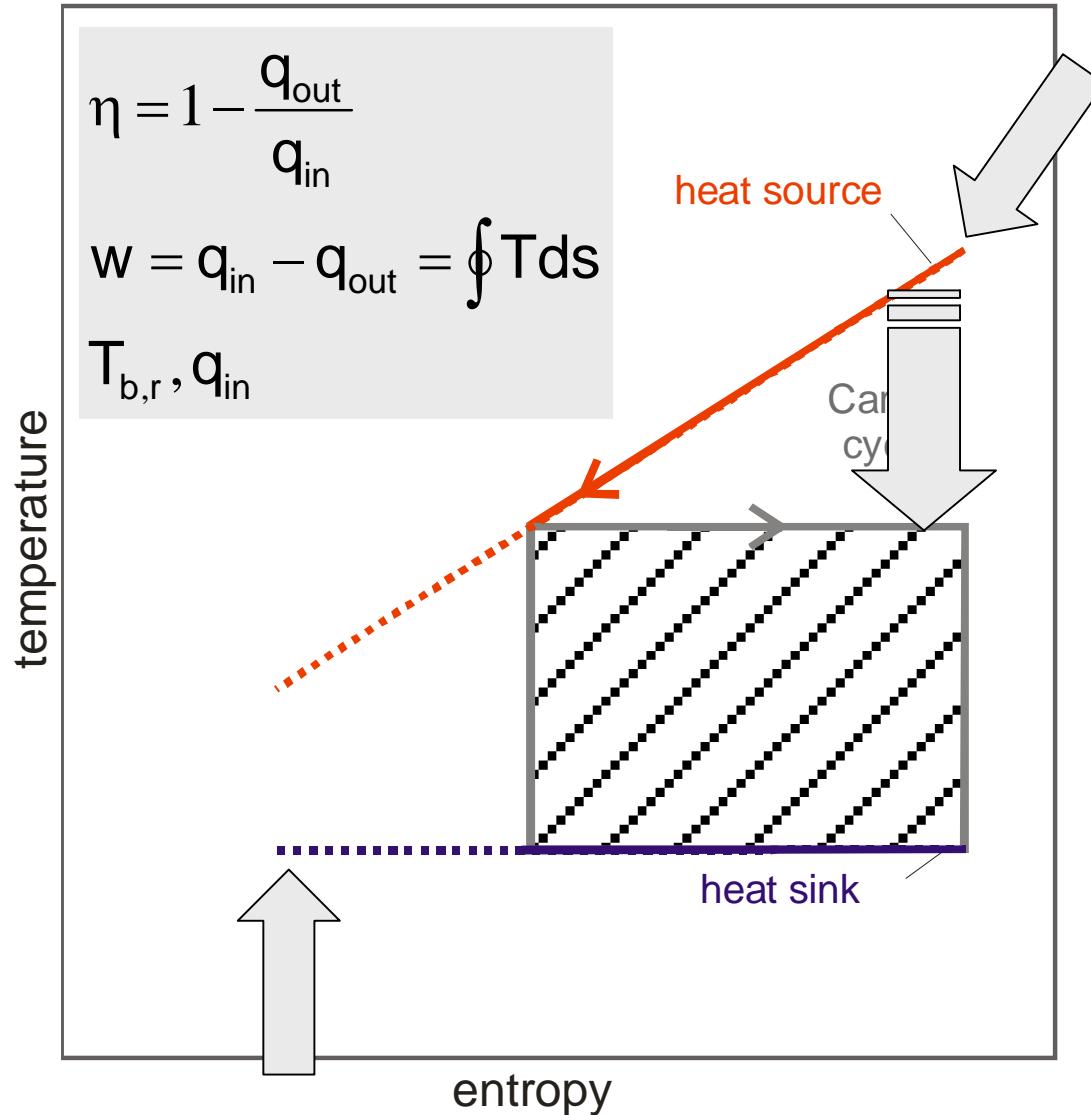
Optimisation of the cycle locates the operating conditions  
for the optimal ideal cycle performance (Tamm et.al.)!

Optimisation approach:

- Locate constraints 
- Locate free variables 
- Define optimisation criterium → objective function
- Find Max / Min by analytical or numerical solving of the function



- $q = \int T ds$
- added heat  $q_{in}: A□A_{23B}$
- rejected heat  $q_{out}: A□A_{14B}$
- $w = q_{in} - q_{out} = \oint T ds$
- Net Work  $w:$   
area  $A□A_{1234}$
- Thermal efficiency  $\eta:$   
area ratio  $\frac{A□A_{1234}}{A□A_{23B}}$



## Constraints

- Brine temperature, mass flow rate
- Heat sink temperature

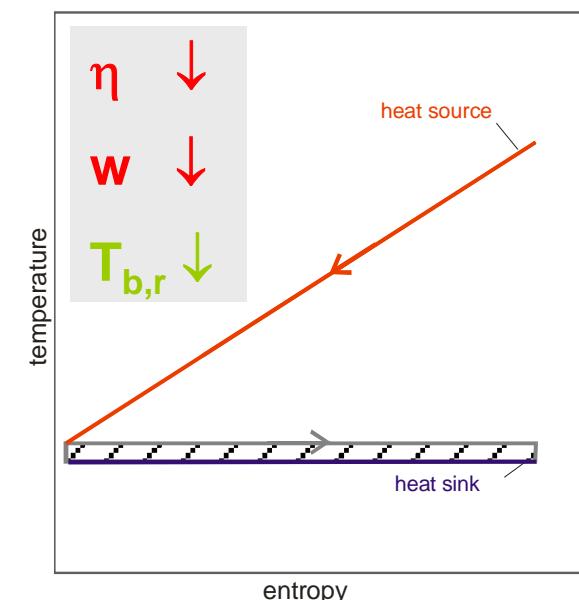
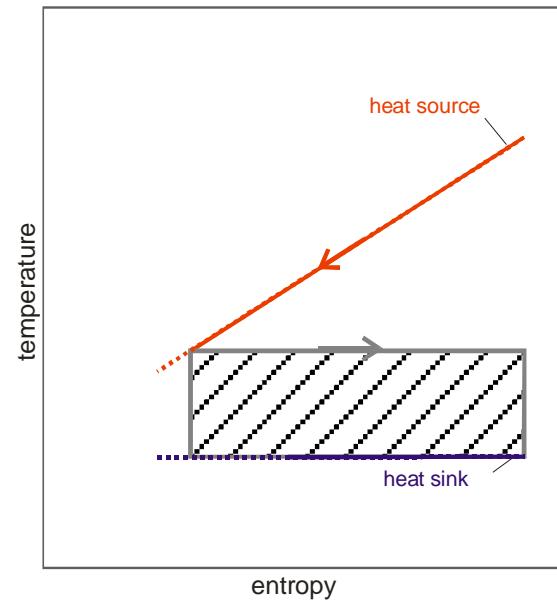
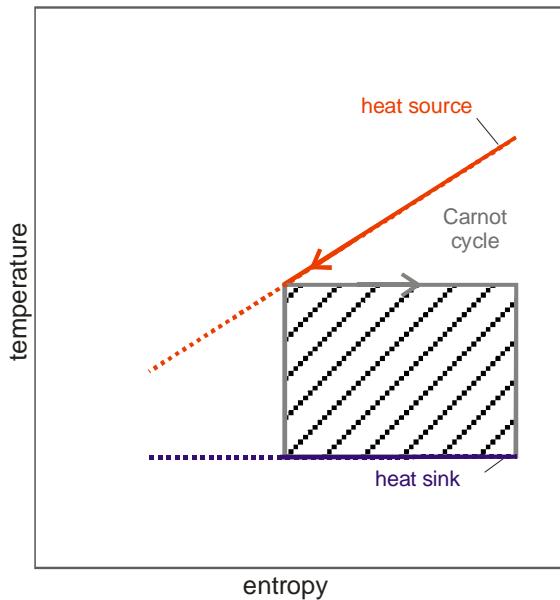
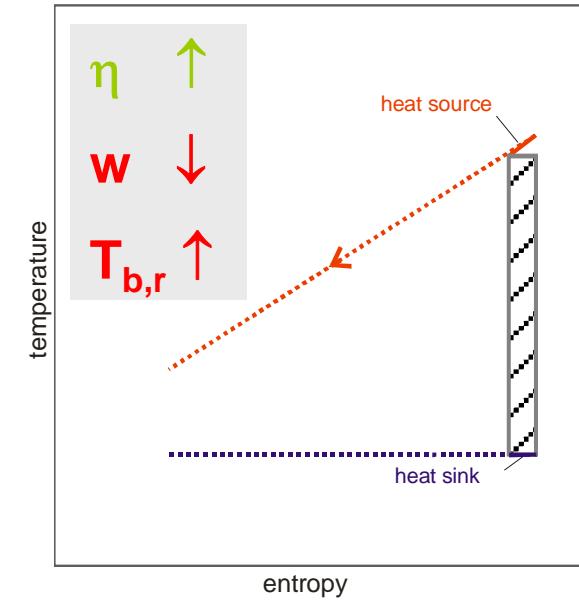
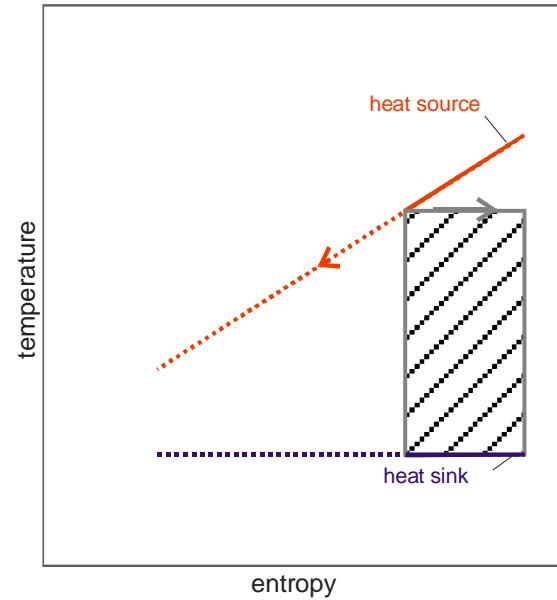
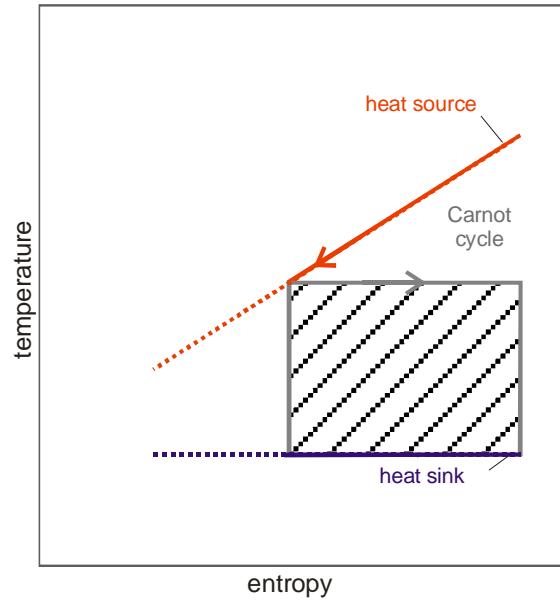
## Free variable

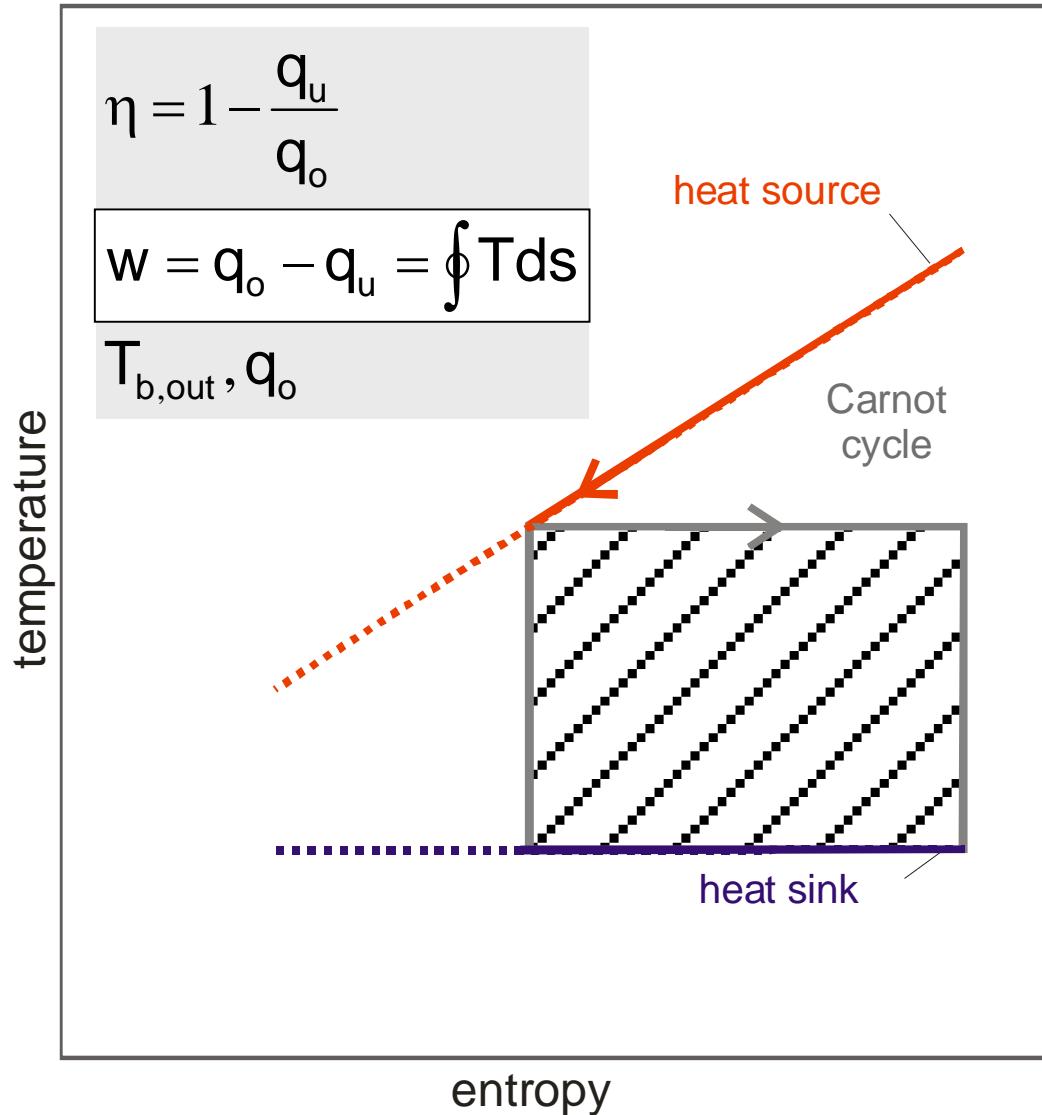
- Upper process temperature  $T_e$

## Possible objective functions

- Thermal efficiency  $\eta$
- Net Work  $w$
- Added heat  $q_{in}$   
/ Cooling of the brine  $T_{b,r}$

# Optimisation of Carnot Cycle





## Constraints

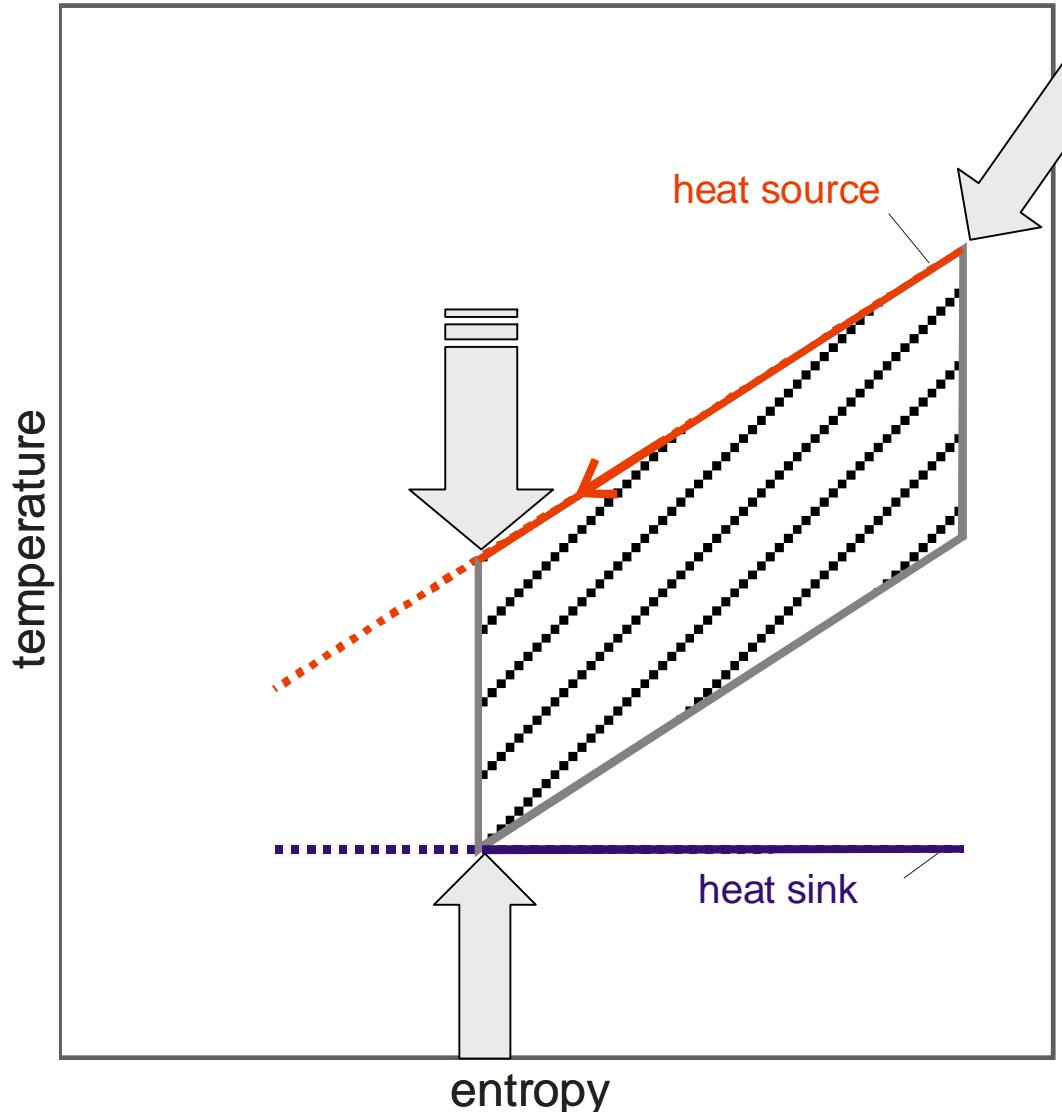
- Brine temperature, mass flow rate
- Heat sink temperature

## Free variable

- Upper process temperature

## Possible objective functions

- Thermal efficiency  $\eta$
- **Net Work w**
- Cooling of the brine  $T_{b,r}$



## Constraints

- Brine temperature, mass flow rate
- Heat sink temperature

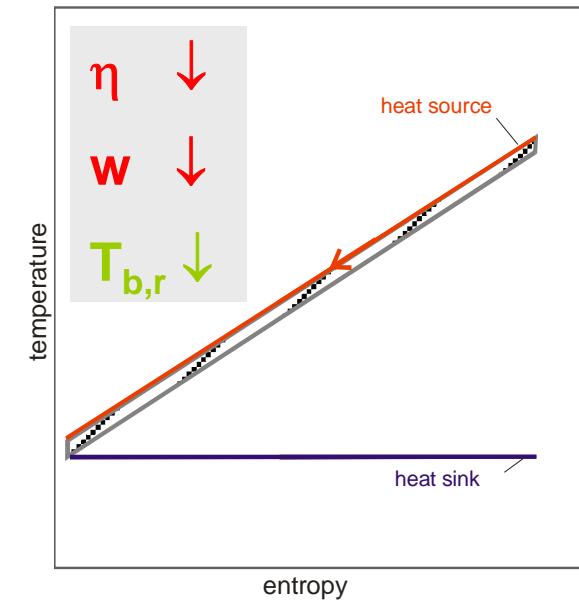
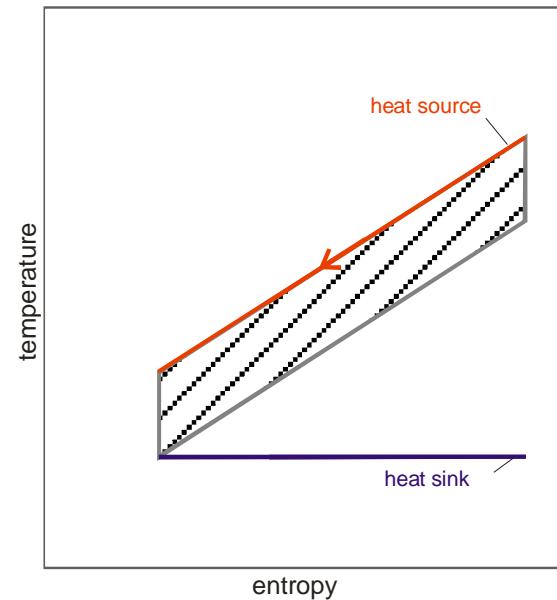
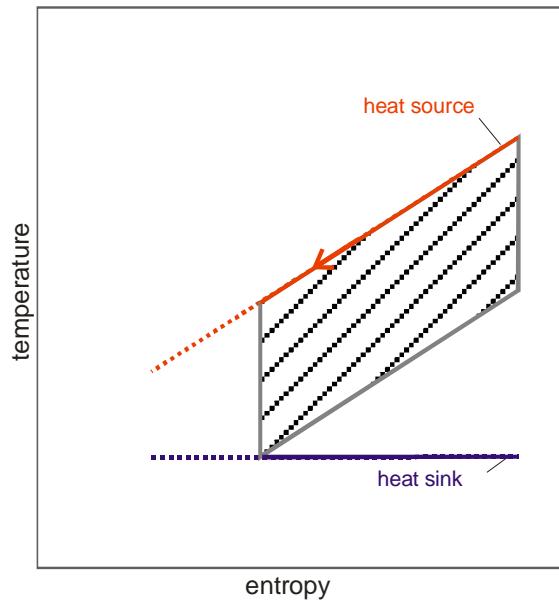
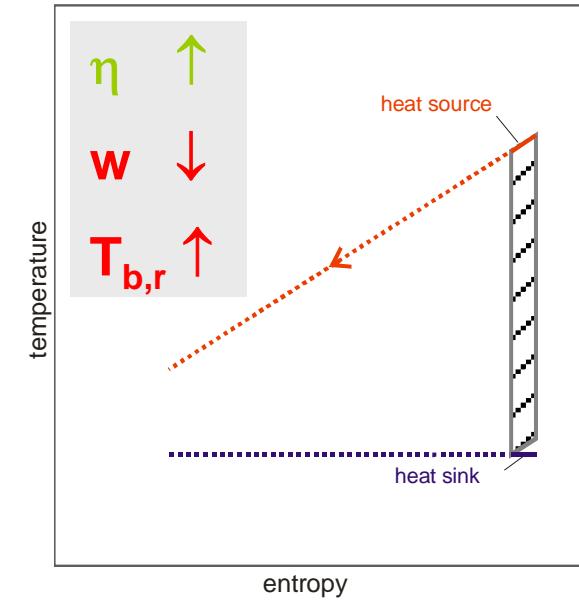
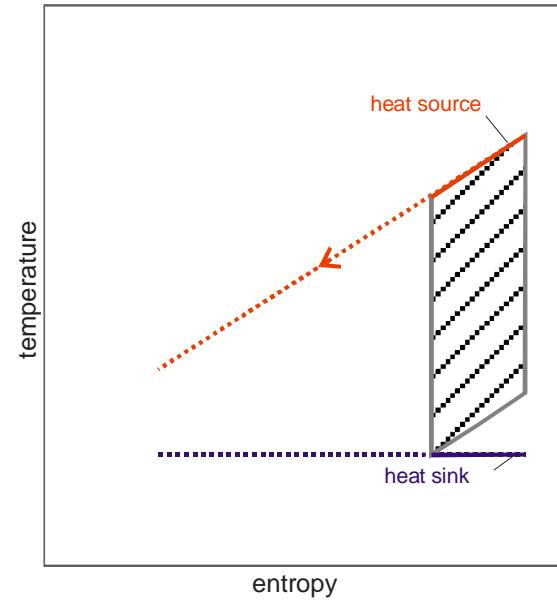
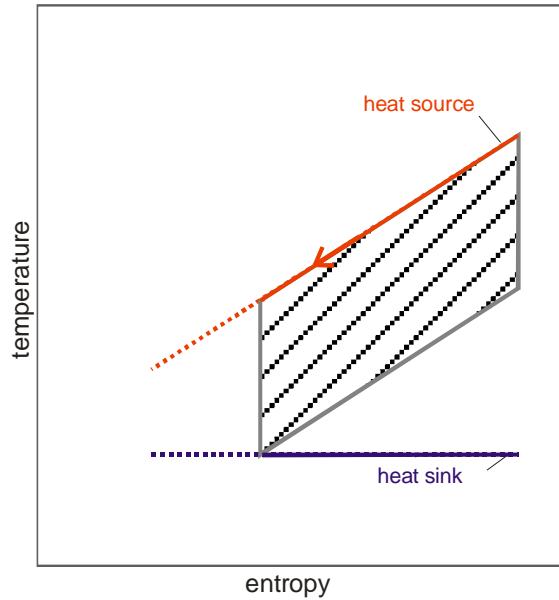
## Free variable

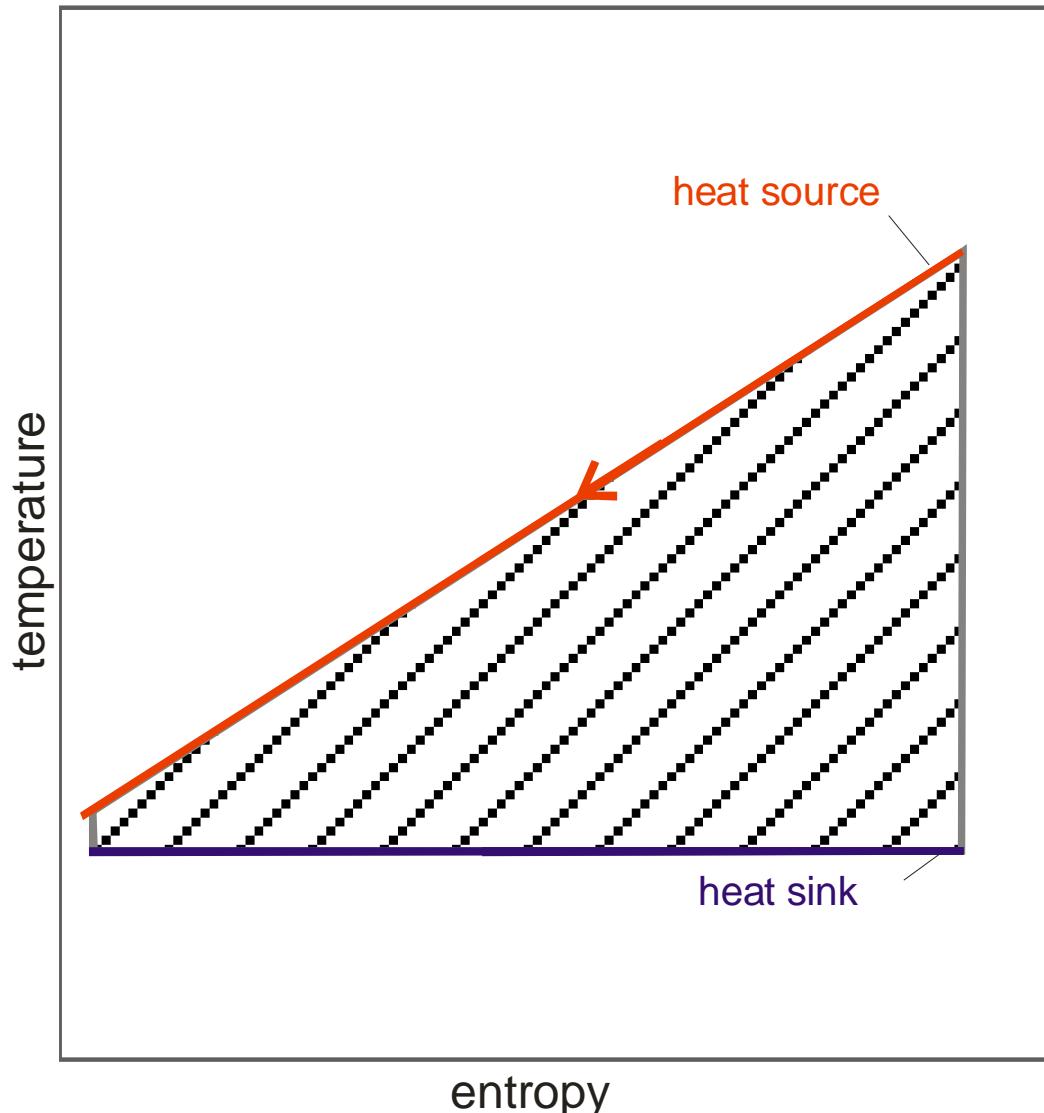
- Upper process temperature  $T_e$

## Possible objective functions

- Thermal efficiency  $\eta$
- Net Work  $w$
- Added heat  $q_{in}$   
/ Cooling of the brine  $T_{b,r}$

# Optimisation of Lorentz Cycle





Fits in heat source / heat sink characteristics

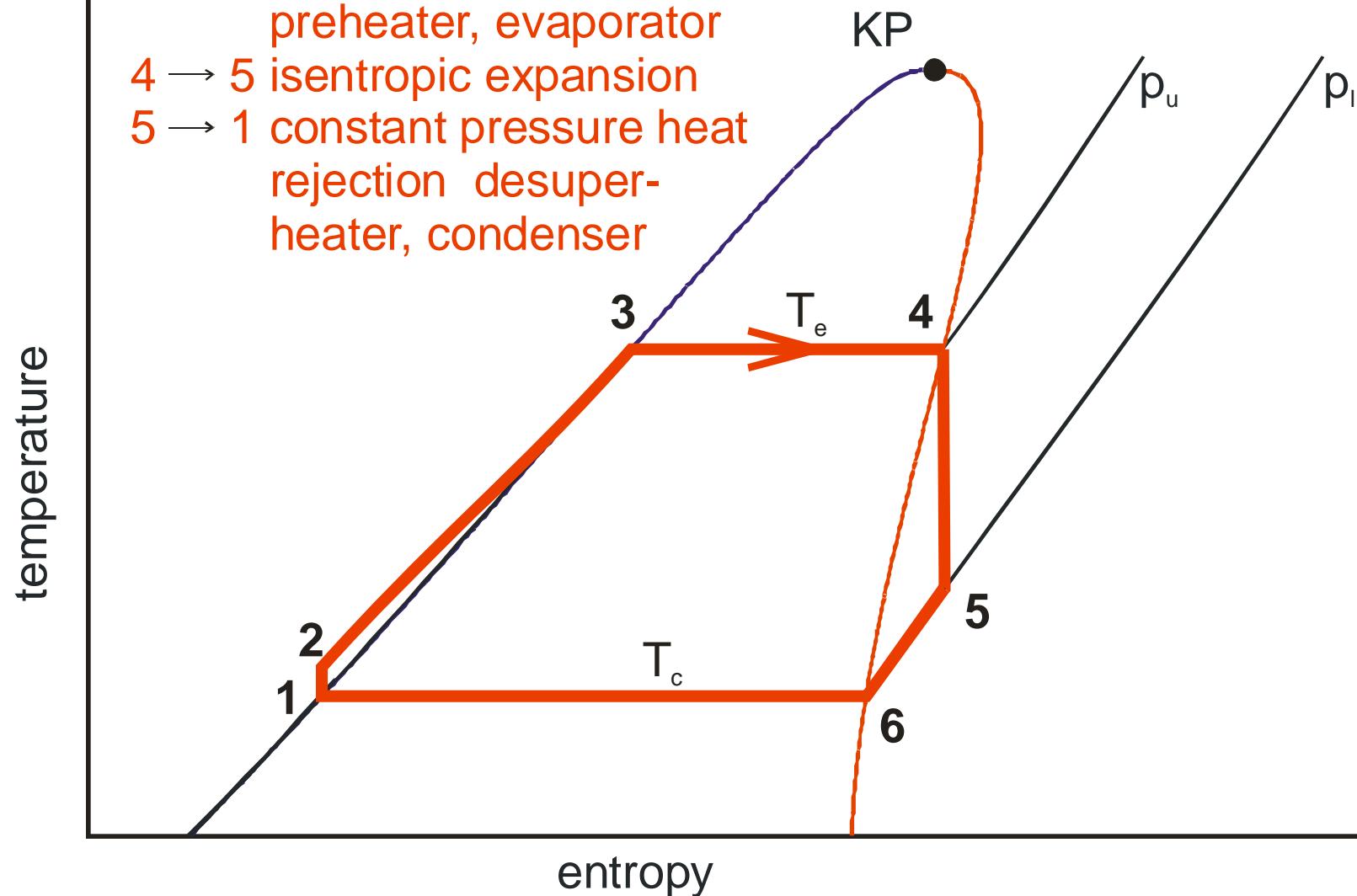
No optimisation

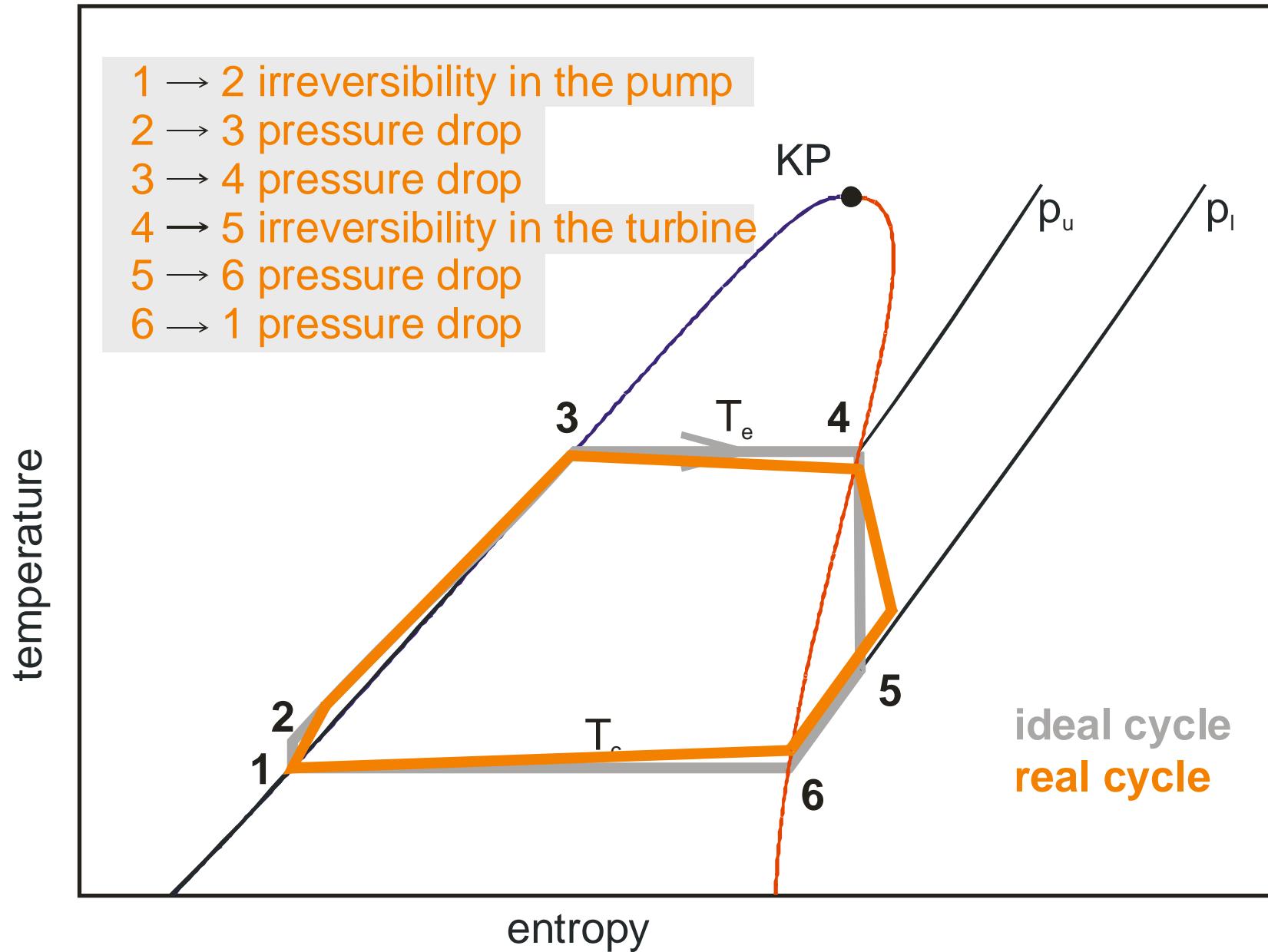
Availability? – not all state changes can be realized with available hard ware

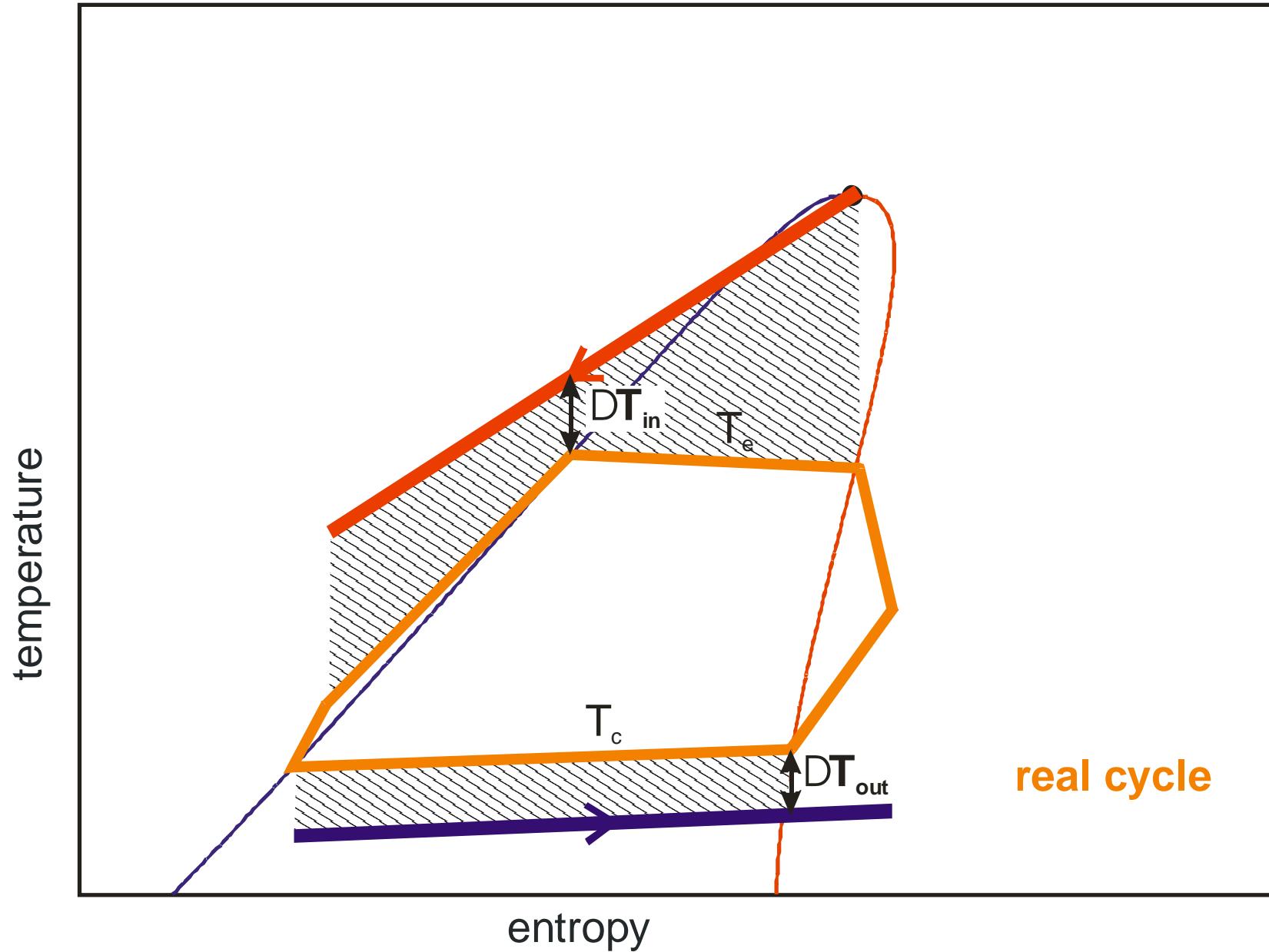
Ideal cycles help to analyse complex problems

Real cycles suffer losses

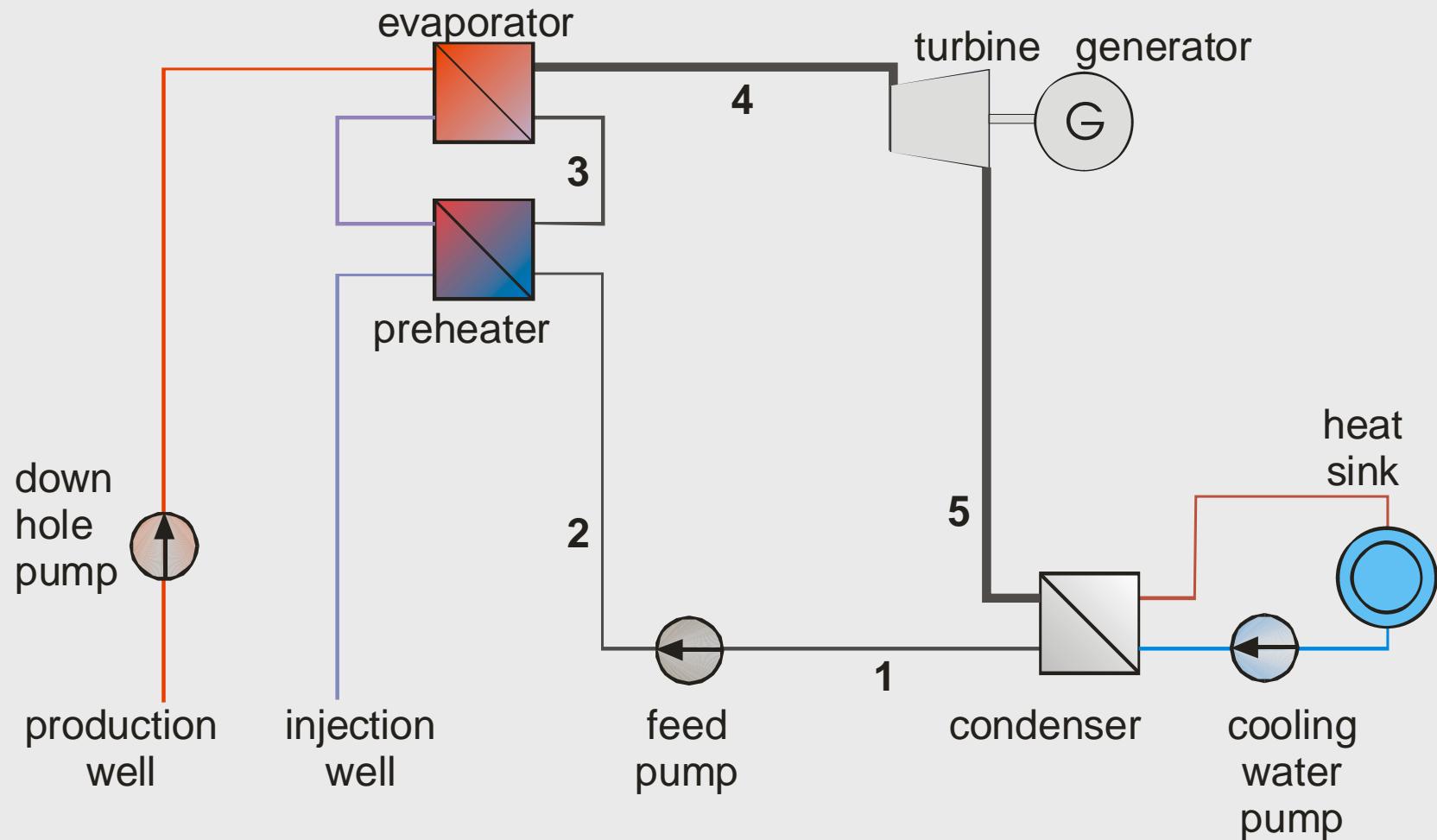
- 1 → 2 isentropic compression
- 2 → 4 constant pressure heat addition  
preheater, evaporator
- 4 → 5 isentropic expansion
- 5 → 1 constant pressure heat rejection  
desuperheater, condenser

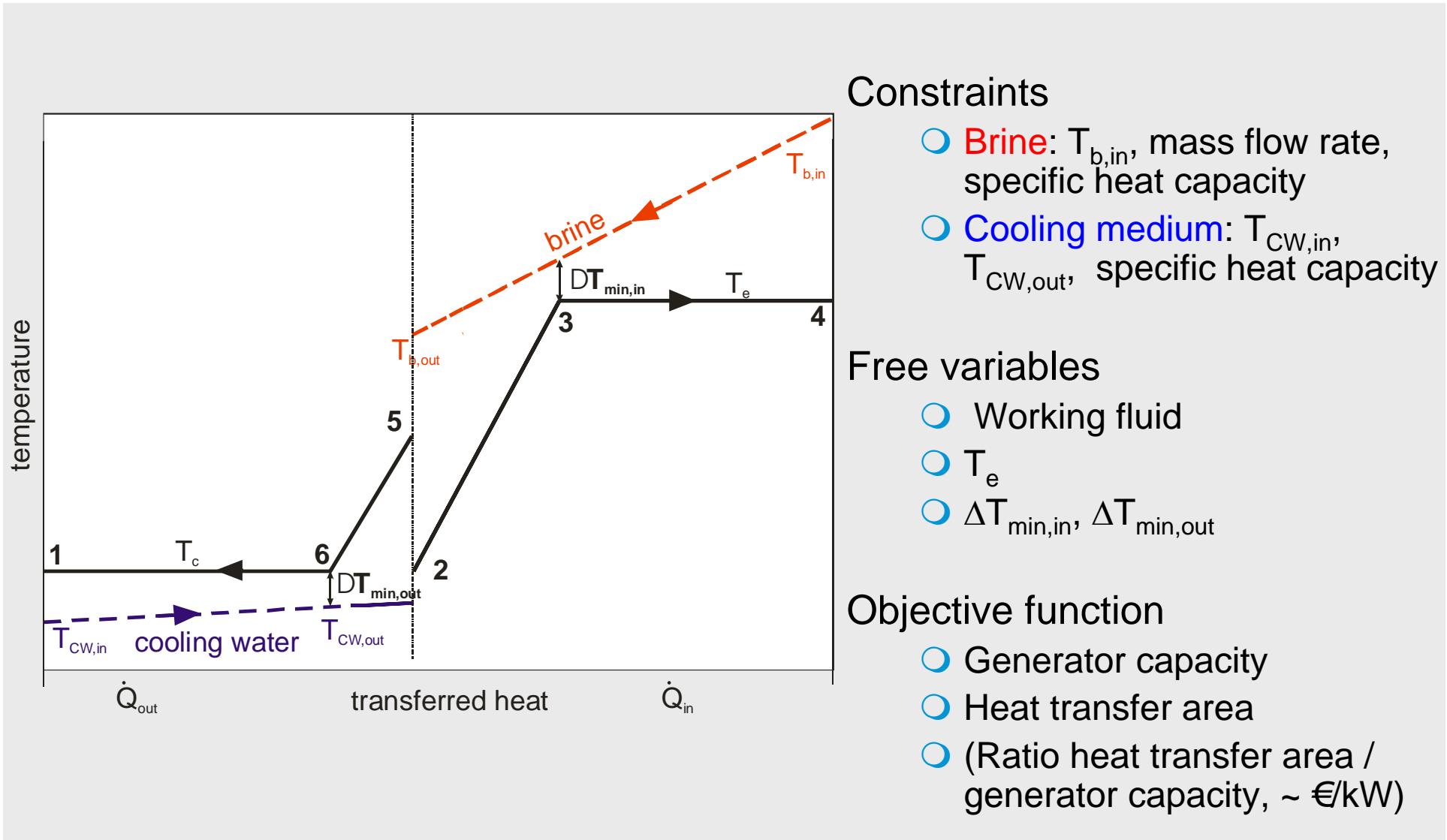


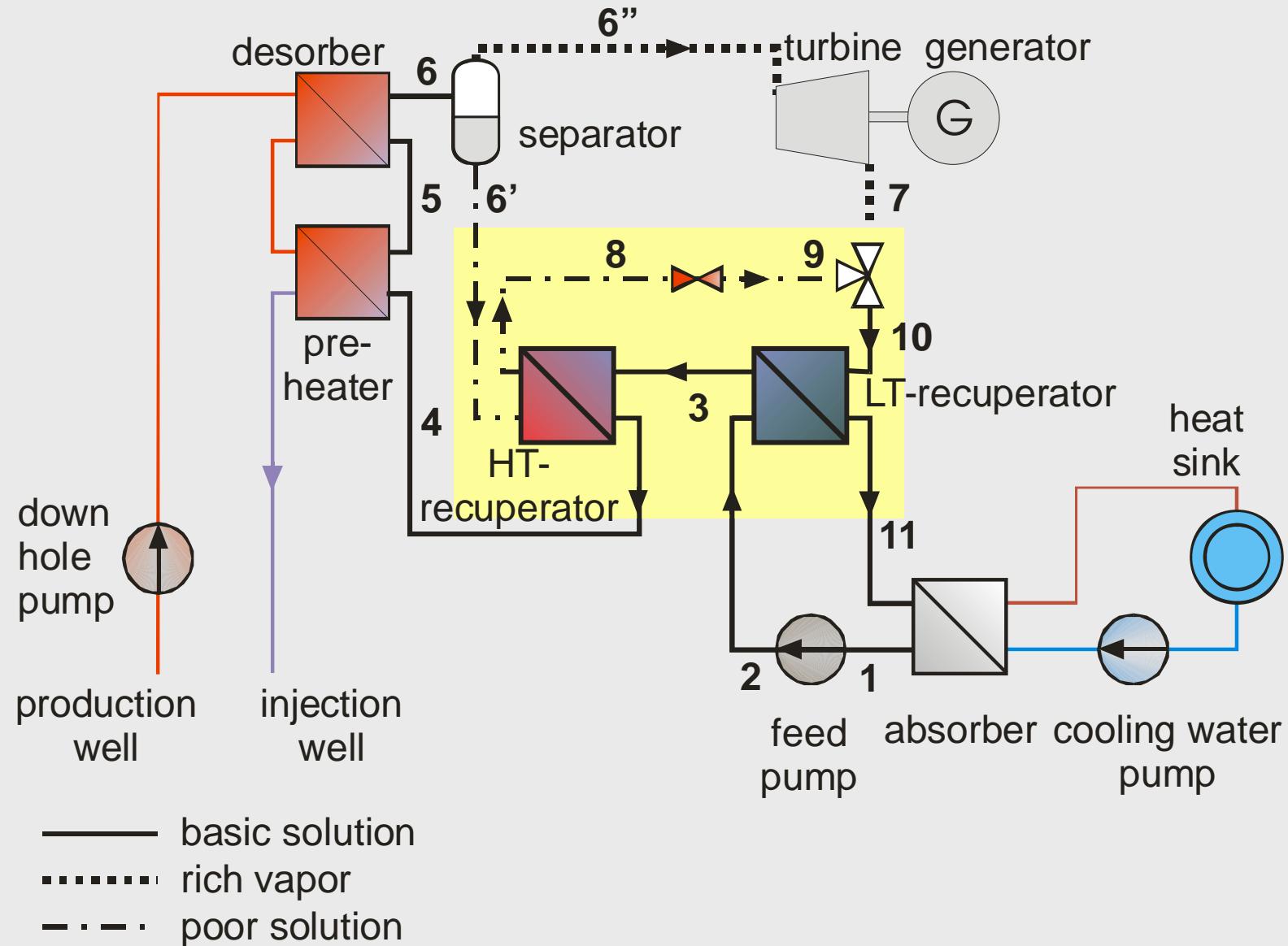




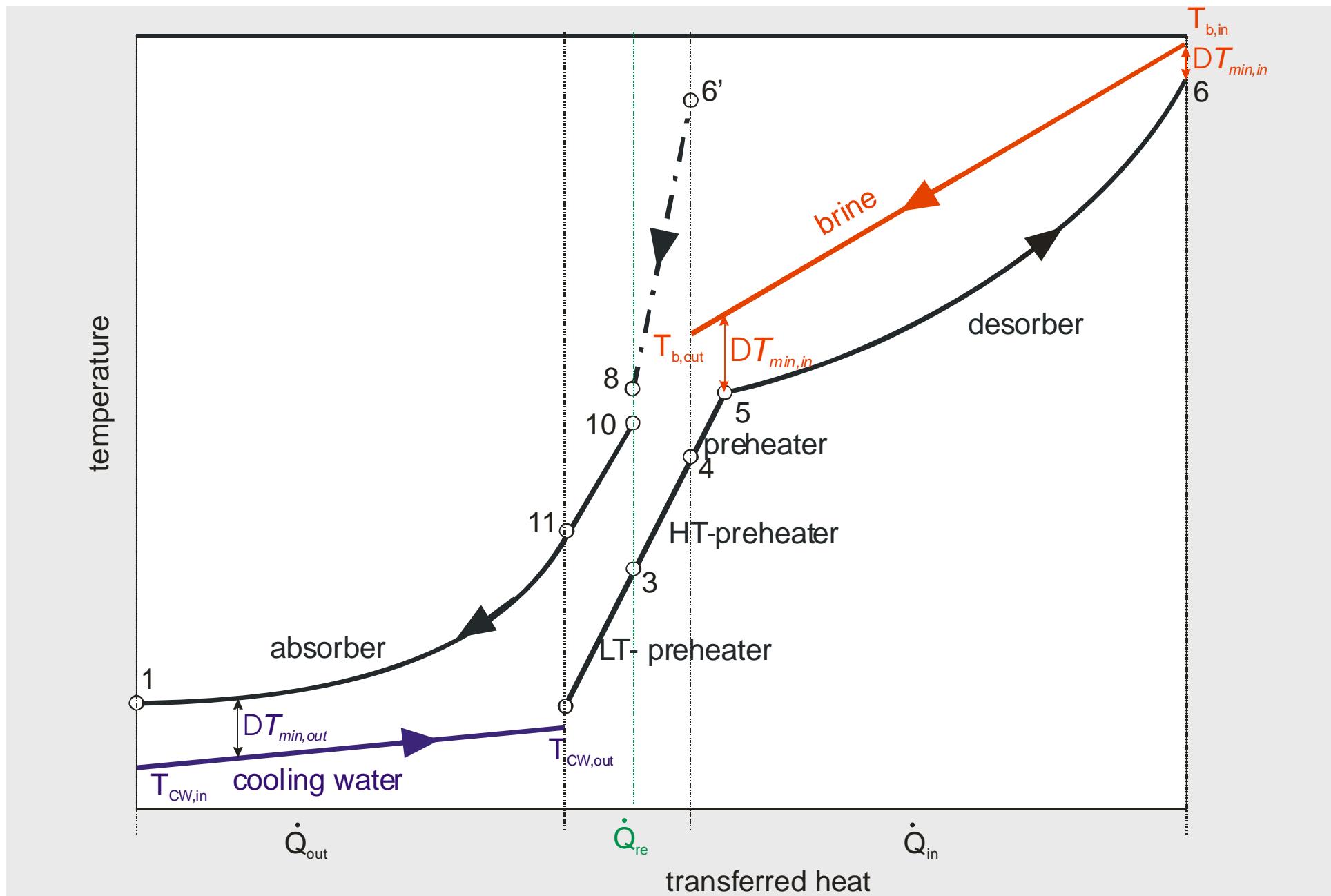
# ORC Layout



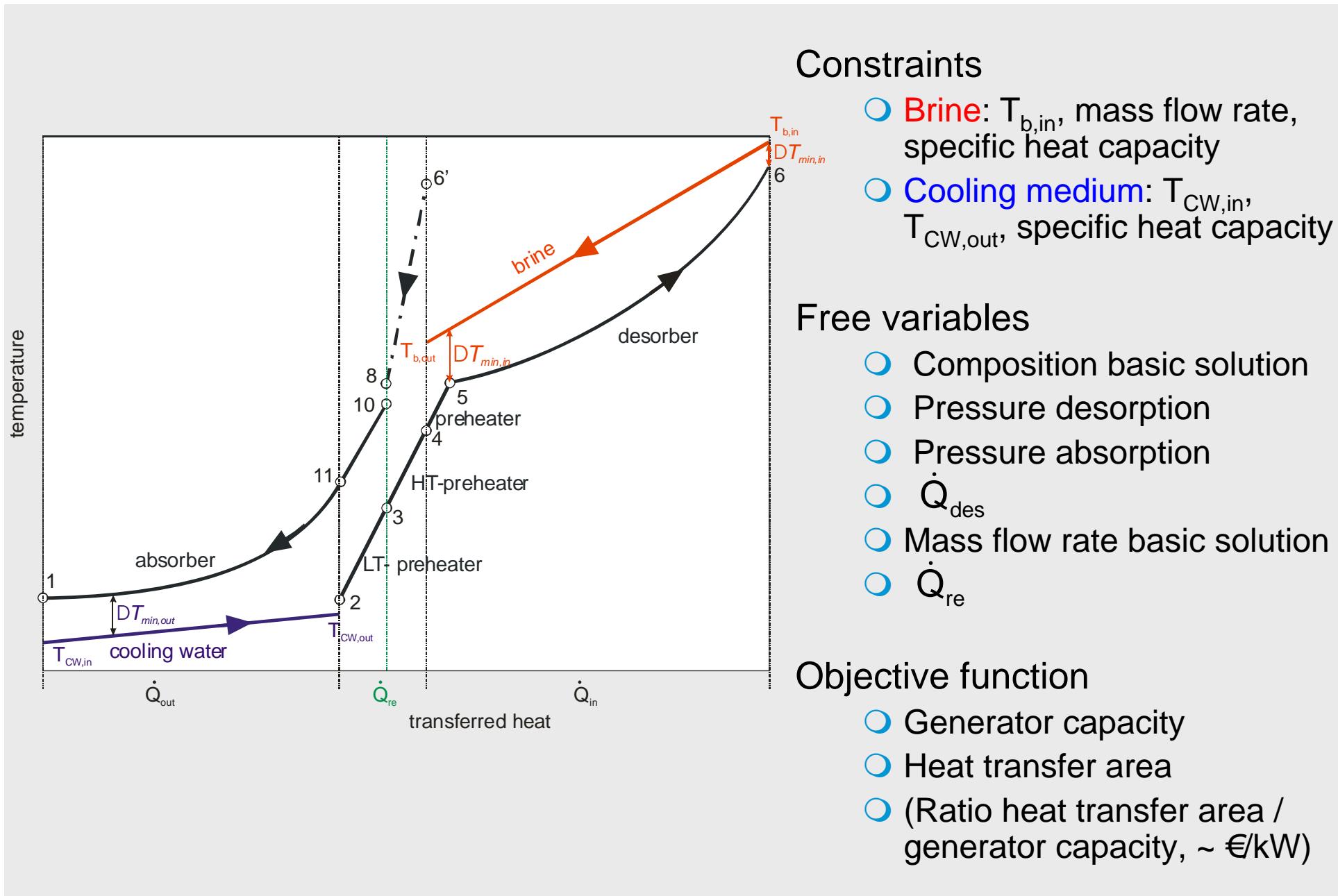




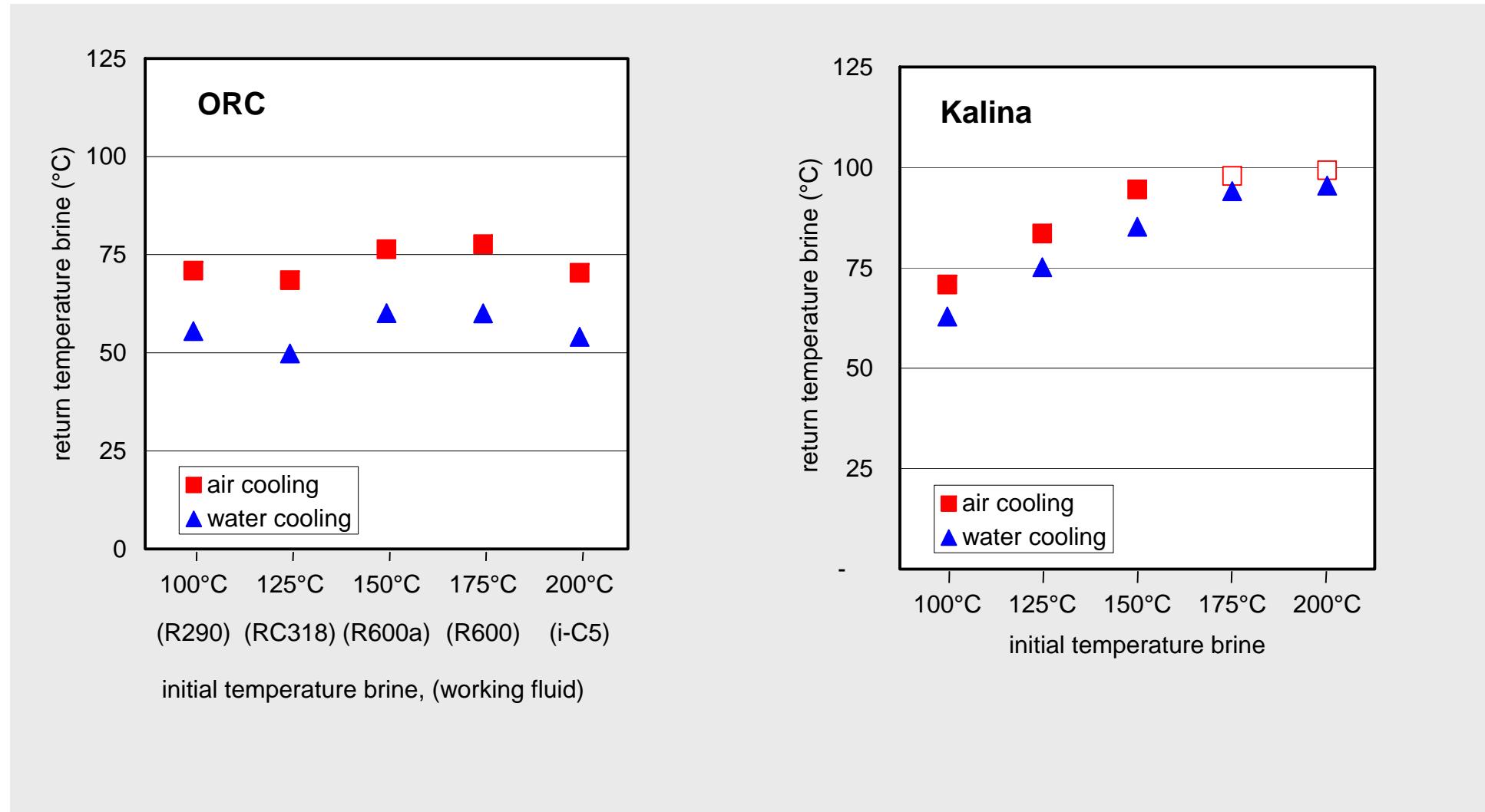
# Heat Transfer Diagram Kalina



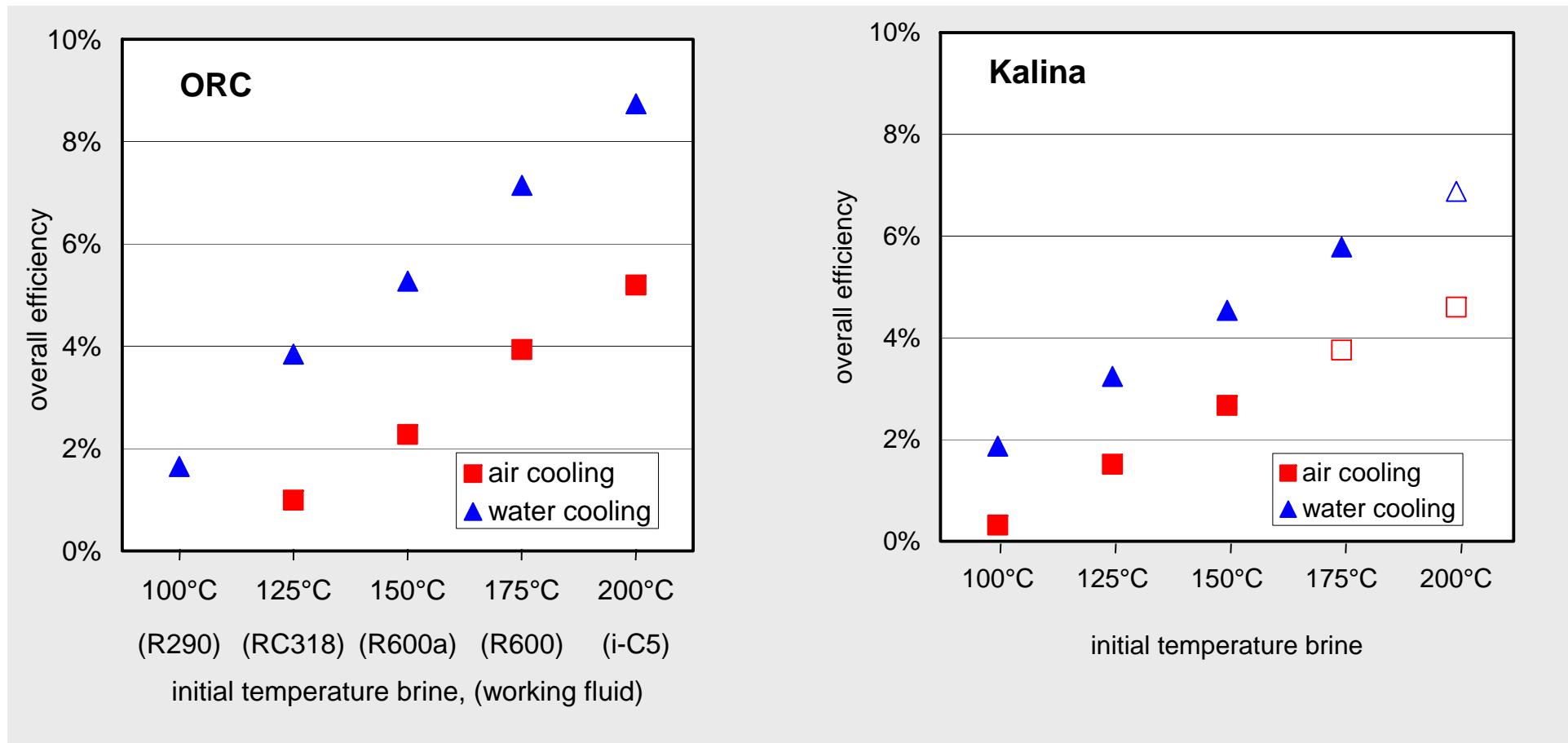
# Heat Transfer Diagram Kalina



Optimised for work output



Optimised for work output



$$\eta_{\text{sys}} = \frac{P_{\text{net}}}{\dot{Q}_{\text{brine}}} = \frac{P_{\text{gen}} - P_{\text{DHpump}} - P_{\text{FeedPump}} - P_{\text{CWpump}}}{\dot{m}_{\text{brine}} c_b (T_{\text{b,in}} - T_0)}$$

Both systems are suitable for power production from low enthalpy reservoirs

With given constraints from heat source and heat sink

- ORC cool the brine more
- Kalina reach higher thermal efficiency
- High parasitic loads at ORC, especially for air cooling
- ORC are more sensible to changes ORC of heat sink

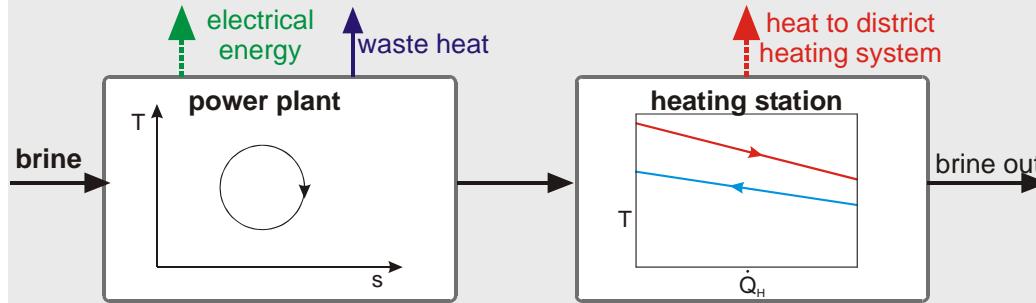
Suitability of the systems

- Kalina KCS34 up to 150 °C brine or CHP
- ORC from 150 °C brine temperature

Improvements

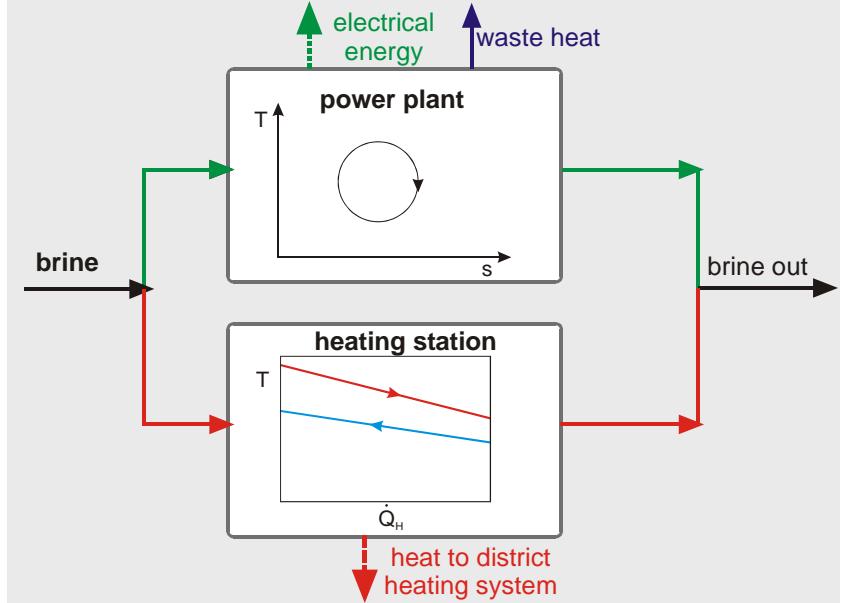
- Supercritical ORC may improve thermal efficiency
- Other Kalina systems may improve cooling of brine

## Serial



- brine temperature > temperature for heating purposes
- Not necessarily simultaneous production

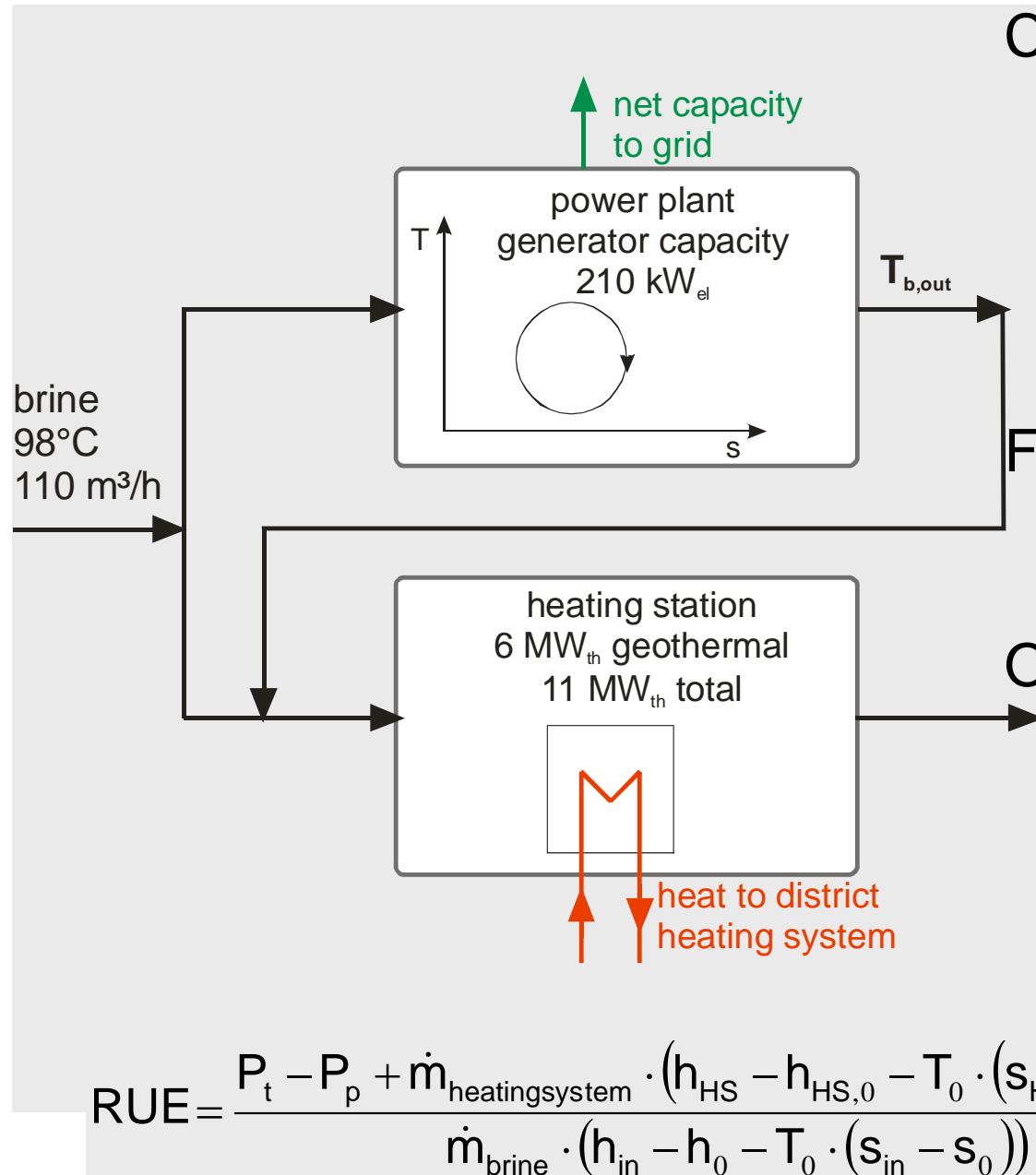
## Parallel



- brine temperature ≈ temperature for heating
- Subsystems compete

Additional constraints due to heating demand!

- Outlet temperature brine
- Mass flow rate brine



## Constraints

- Brine temperature, mass flow rate
- Heat sink temperature
- Heating capacity in district heating system

## Free variable

- Portion of brine through plant / upper process temperature

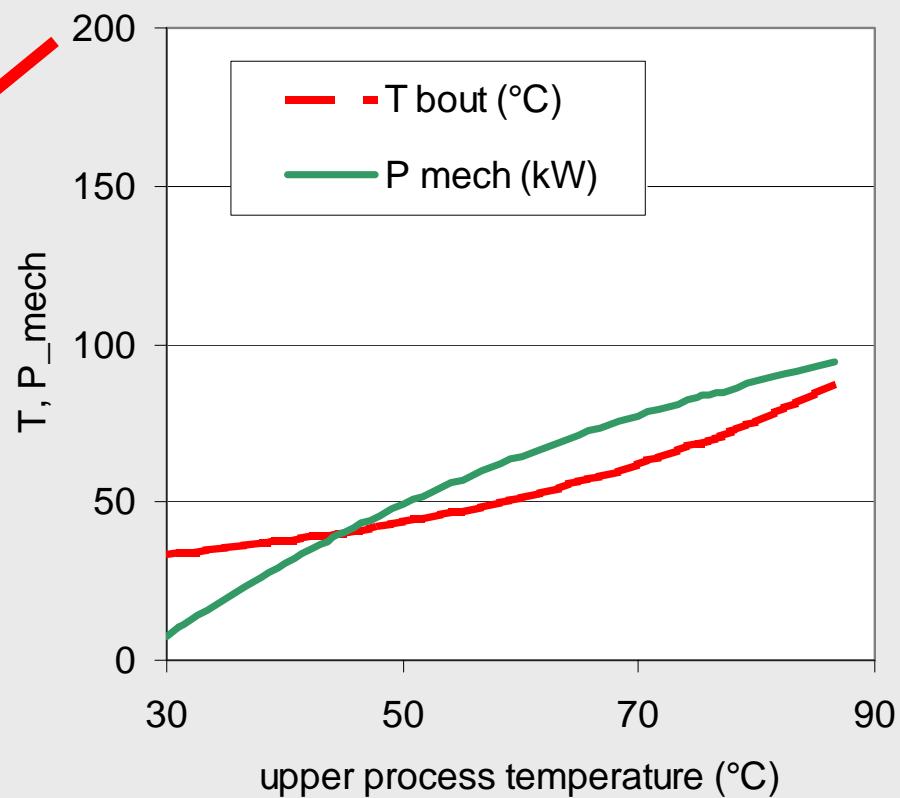
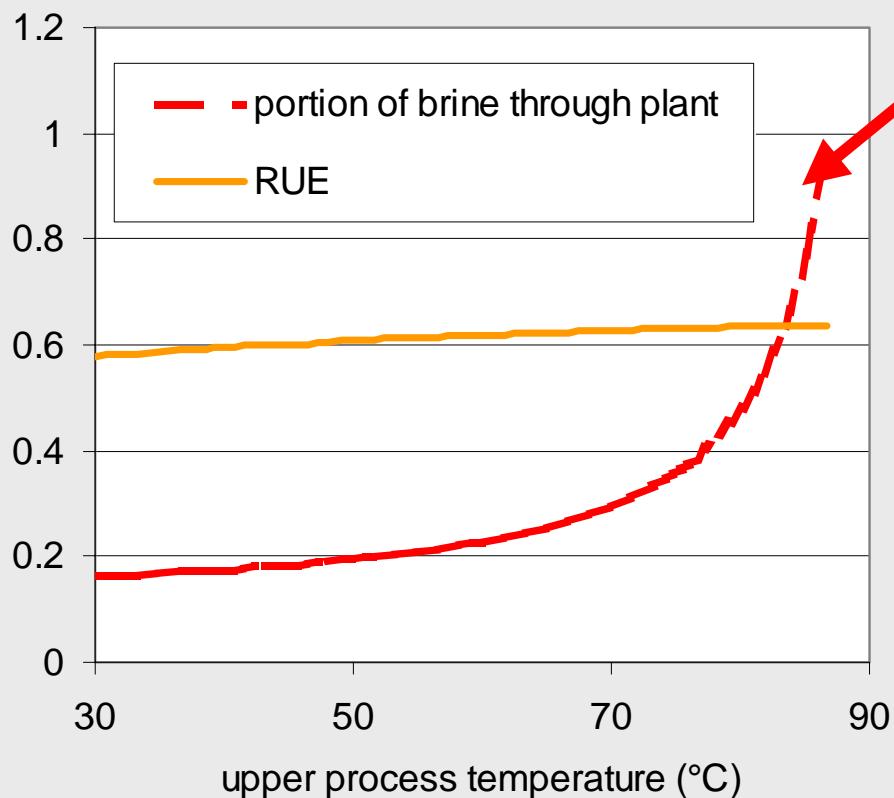
## Objective functions

- Generator capacity  $\sim P_{\text{mech}}$
- Cooling of the brine  $T_{\text{b,out}}$
- Resource Utilization Factor **RUE** (overall exergetic efficiency)

$$\text{RUE} = \frac{P_t - P_p + \dot{m}_{\text{heatingsystem}} \cdot (h_{\text{HS}} - h_{\text{HS},0} - T_0 \cdot (s_{\text{HS}} - s_{\text{HS},0}))}{\dot{m}_{\text{brine}} \cdot (h_{\text{in}} - h_0 - T_0 \cdot (s_{\text{in}} - s_0))}$$

# Results of Optimisation

- Brine 35 kg/s, 98 °C
- District heating system (assumed) 50 kg/s, 70/55, 3.1 MW<sub>th</sub>
- Working medium power plant Perflourpentane, water cooling 15/20



$$\dot{Q}_{in} = \text{const} = \dot{m}_{\text{brine}} c \cdot (T_{b,in} - T_{b,out})$$

ORC & Kalina follow the same rules, but deal differently with the losses.

## Losses

- Irreversible heat transfer
- Internal irreversibilities (non-isentropic state changes turbine and pump, pressure losses)
- Parasitic loads (cycle pump, down hole pump, cooling devices)

## Constraints

- Heat source and heat sink

## Free Variables

- Layout
- Working fluid (medium, composition)
- Upper process temperature

Power plant: optimised for work output

CHP: optimised for RUE