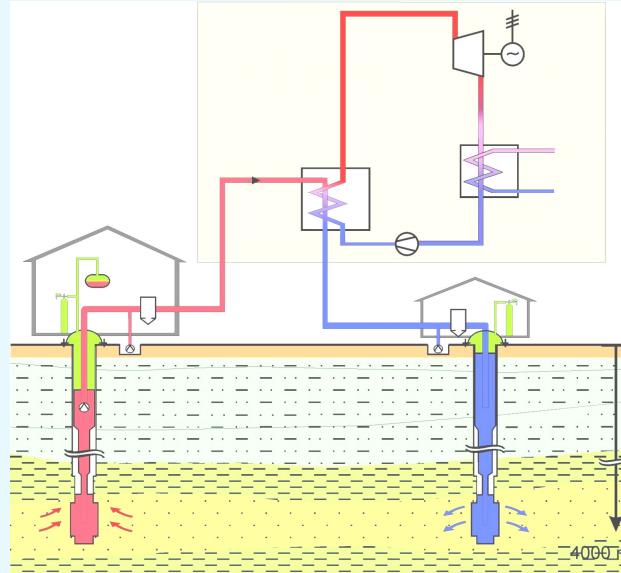


DESIGN OF GEOTHERMAL POWER PLANTS

holistic approach considering auxiliary power



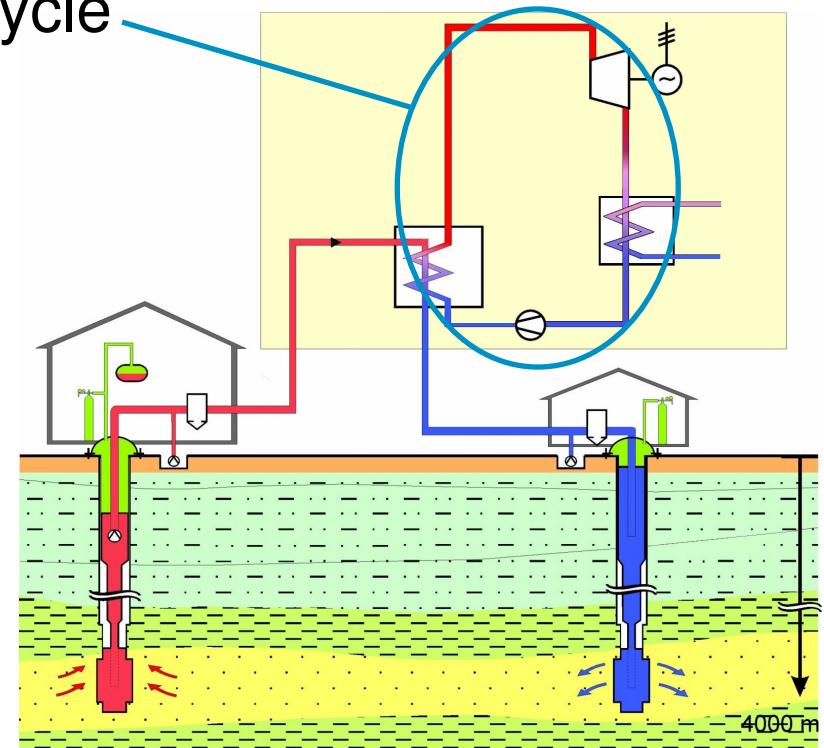
Stephanie Frick, Ali Saadat, Stefan Kranz

GeoForschungsZentrum Potsdam



ENGINE Final Conference
Vilnius, Lithuania
12-15 February 2008

- Power plants serve for net power production
- Net power = gross power - auxiliary power
- Auxiliary power {conversion cycle



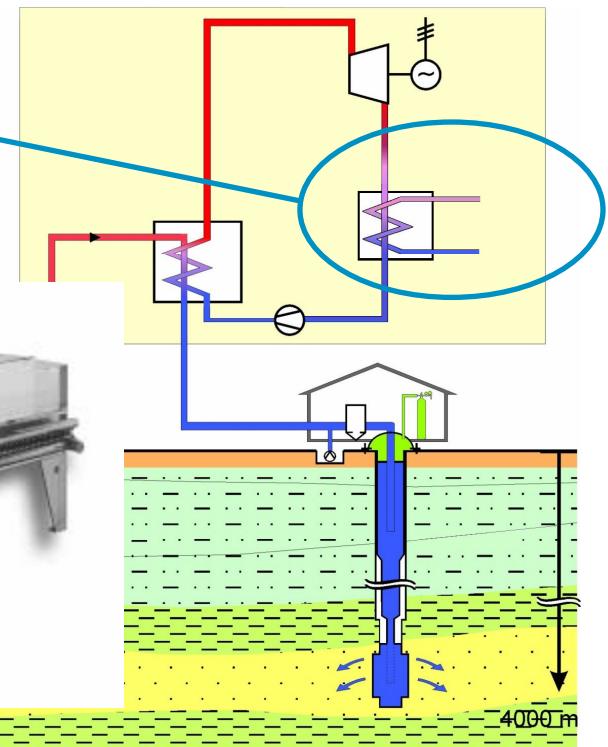
- Power plants serve for net power production
- Net power = gross power - auxiliary power
- Auxiliary power {conversion cycle
cooling cycle



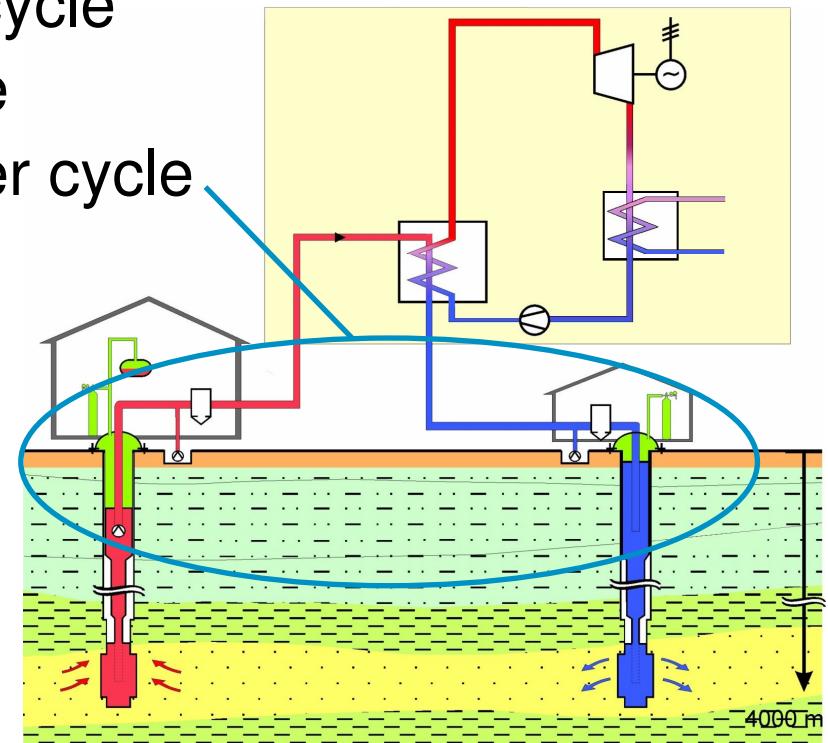
source: <http://www.erdwaerme-kraft.de/>



source: <http://www.refplus.com/>



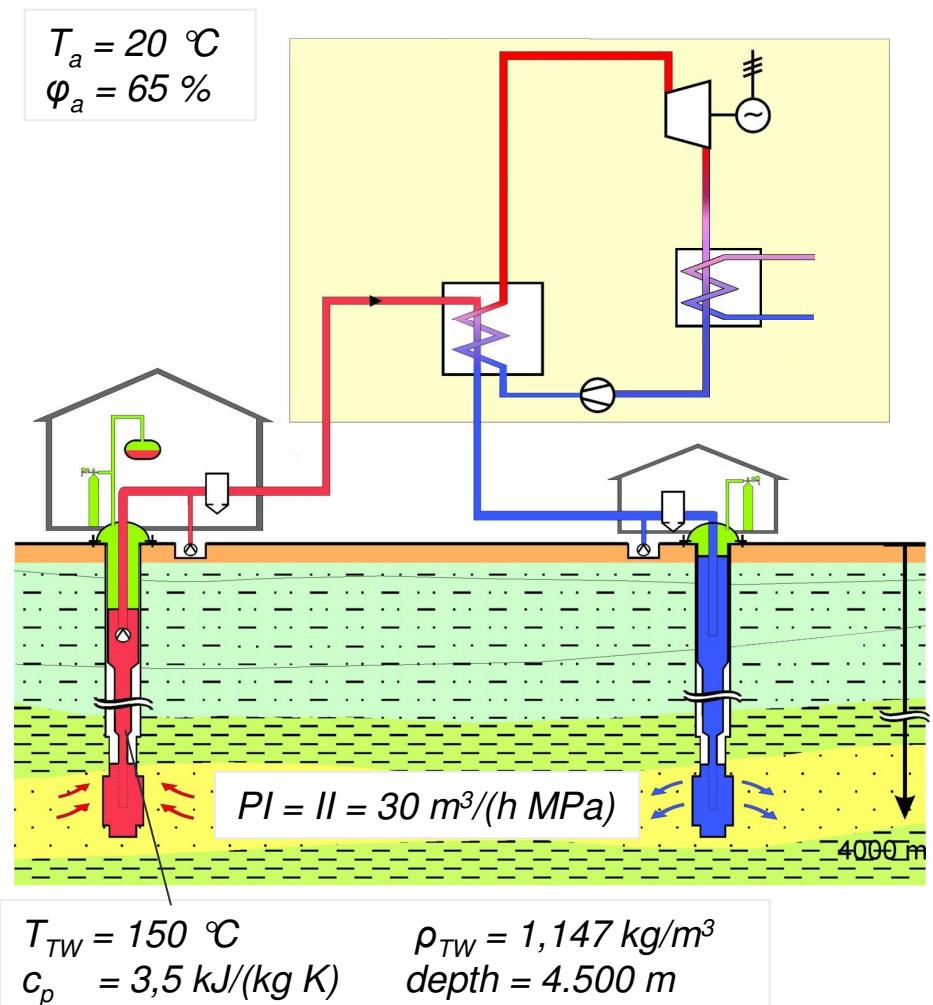
- Power plants serve for net power production
- Net power = gross power - auxiliary power
- Auxiliary power {conversion cycle
cooling cycle
thermal water cycle}



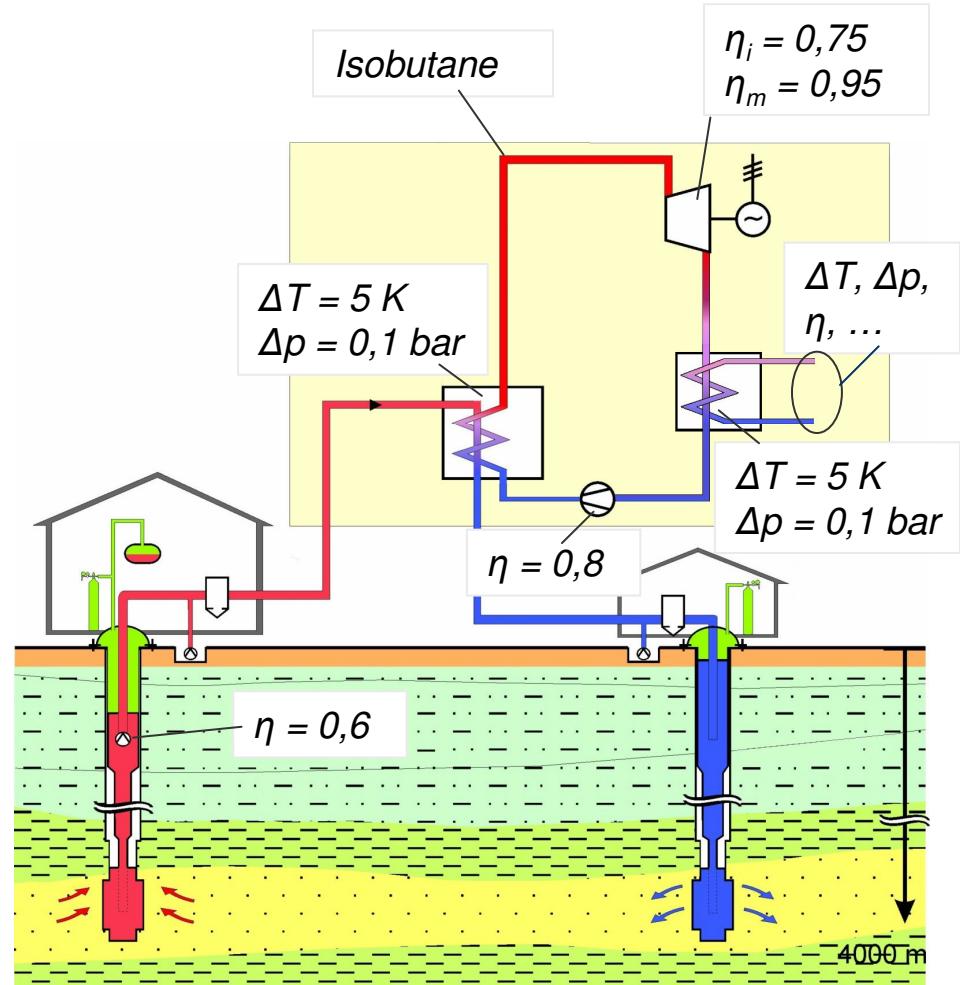
- Power plants serve for net power production
 - Net power = gross power - auxiliary power
 - Auxiliary power { conversion cycle
cooling cycle
thermal water cycle
- For geothermal power plants, a maximum net power output can't be reached by maximising the gross power
- Geothermal power plant design needs a holistic approach

- Methodical approach to power plant design
- Gross power characteristics
- Auxiliary power characteristics
- Practical approach to power plant design
- Conclusions & Outlook

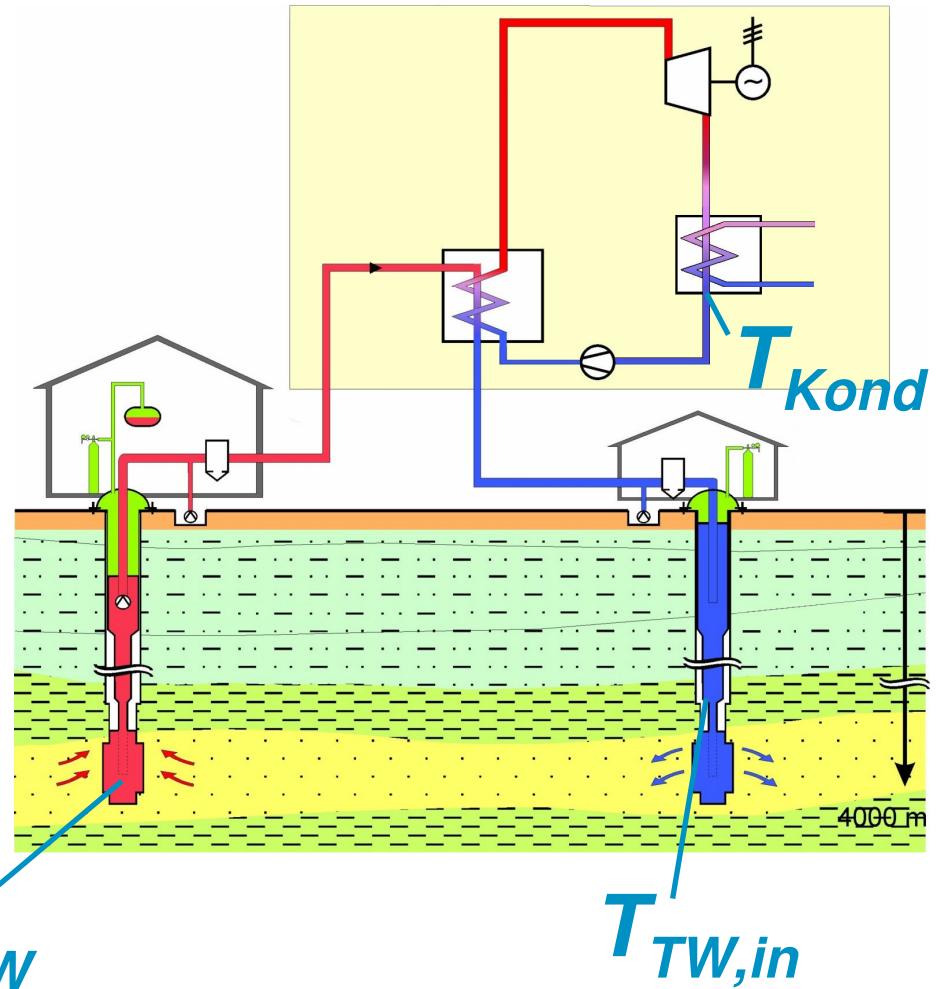
- site-specific reservoir characteristics and ambient conditions
(→ boundary conditions)



- site-specific reservoir characteristics and ambient conditions
(→ boundary conditions)
- plant-specific parameters
(→ component quality)

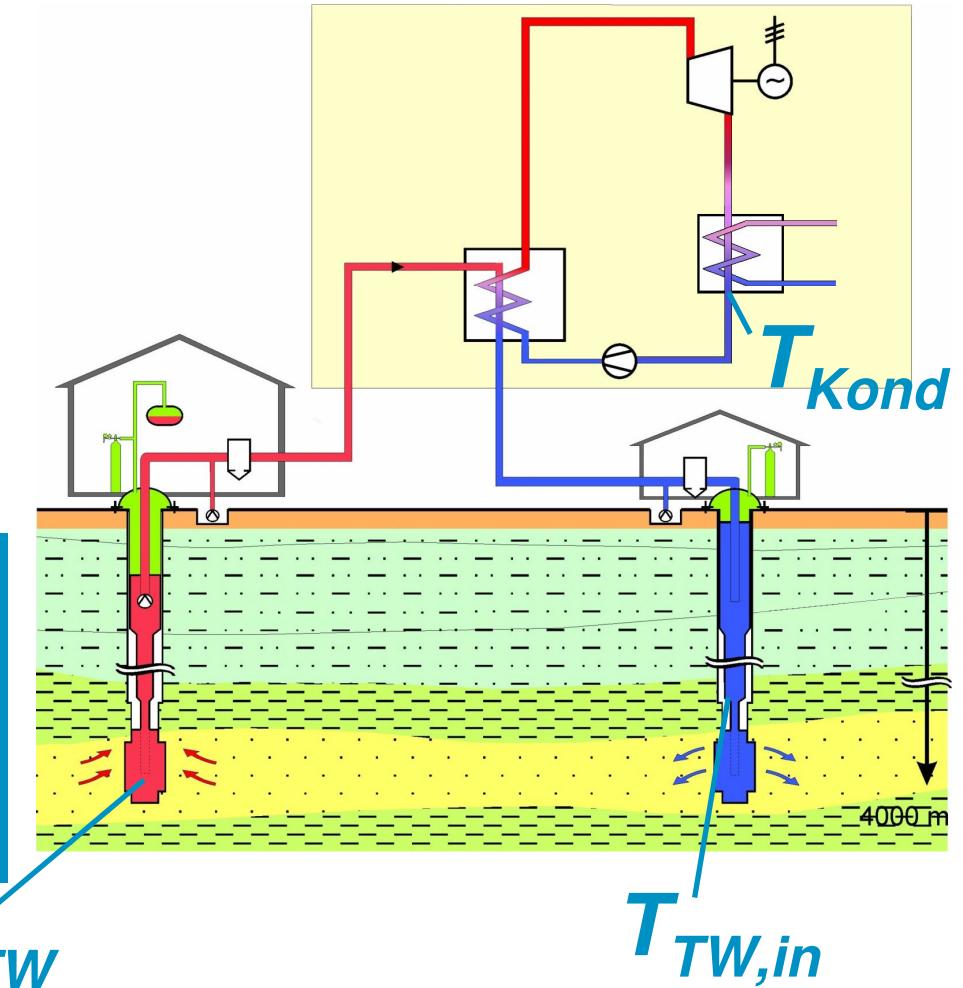


- site-specific reservoir characteristics and ambient conditions
(→ boundary conditions)
- plant-specific parameters
(→ component quality)
- **design parameters:**
condensation temp. T_{Kond}
injection temperature $T_{TW,in}$
thermal water mass flow \dot{m}_{TW}



- site-specific reservoir characteristics and ambient conditions
(→ boundary conditions)
- plant-specific parameters
(→ component quality)
- design parameters:

What influence have the design parameters on power plant performance?



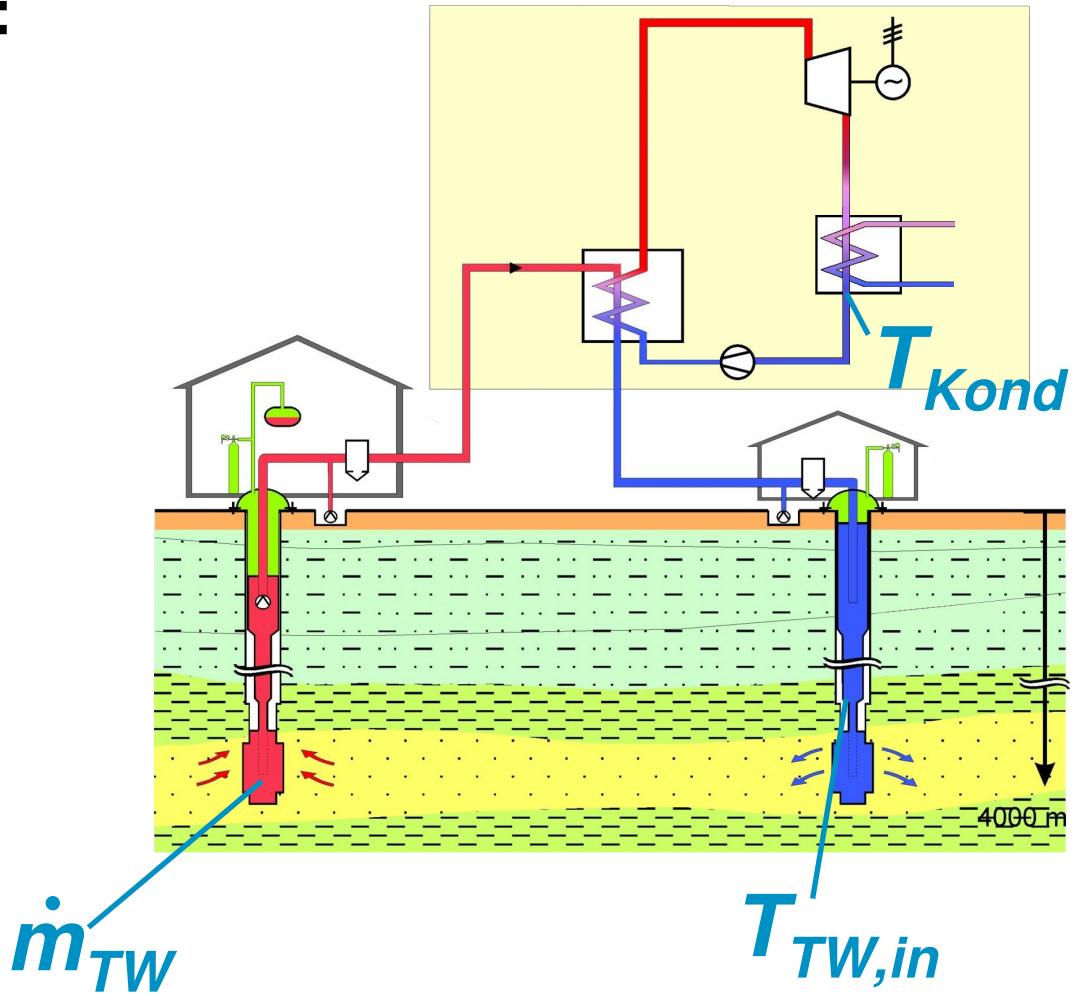
Exemplary power plant in the North German Basin:

$$T_{TW} = 150 \text{ } ^\circ\text{C}$$

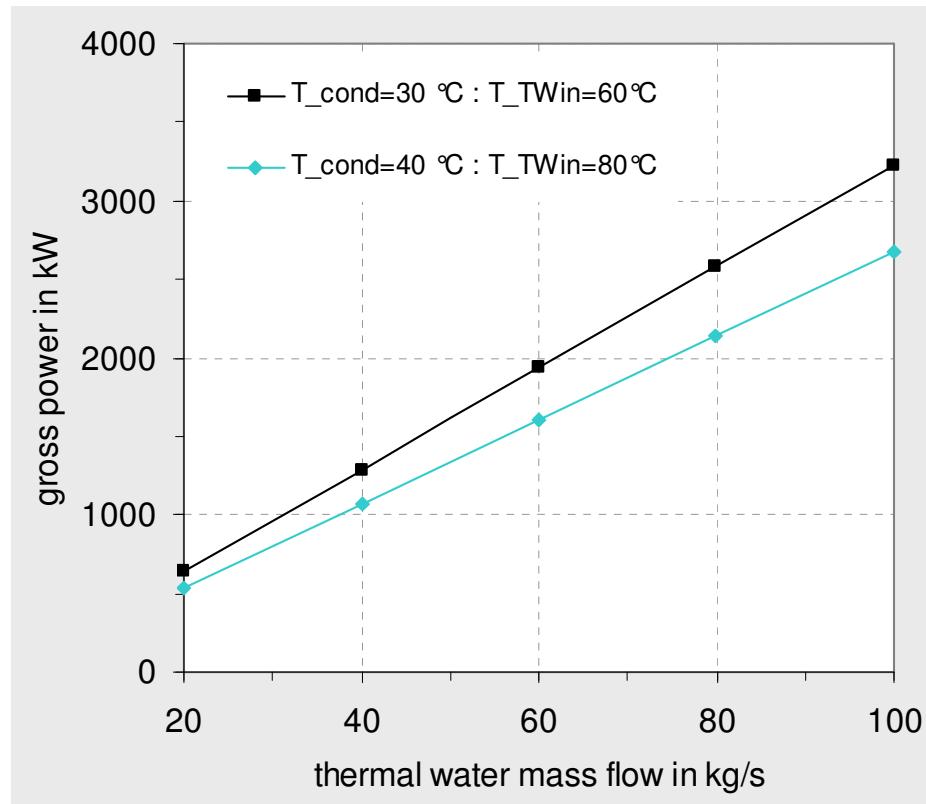
$$PI = 30 \text{ } m^3/(h \text{ MPa})$$

...

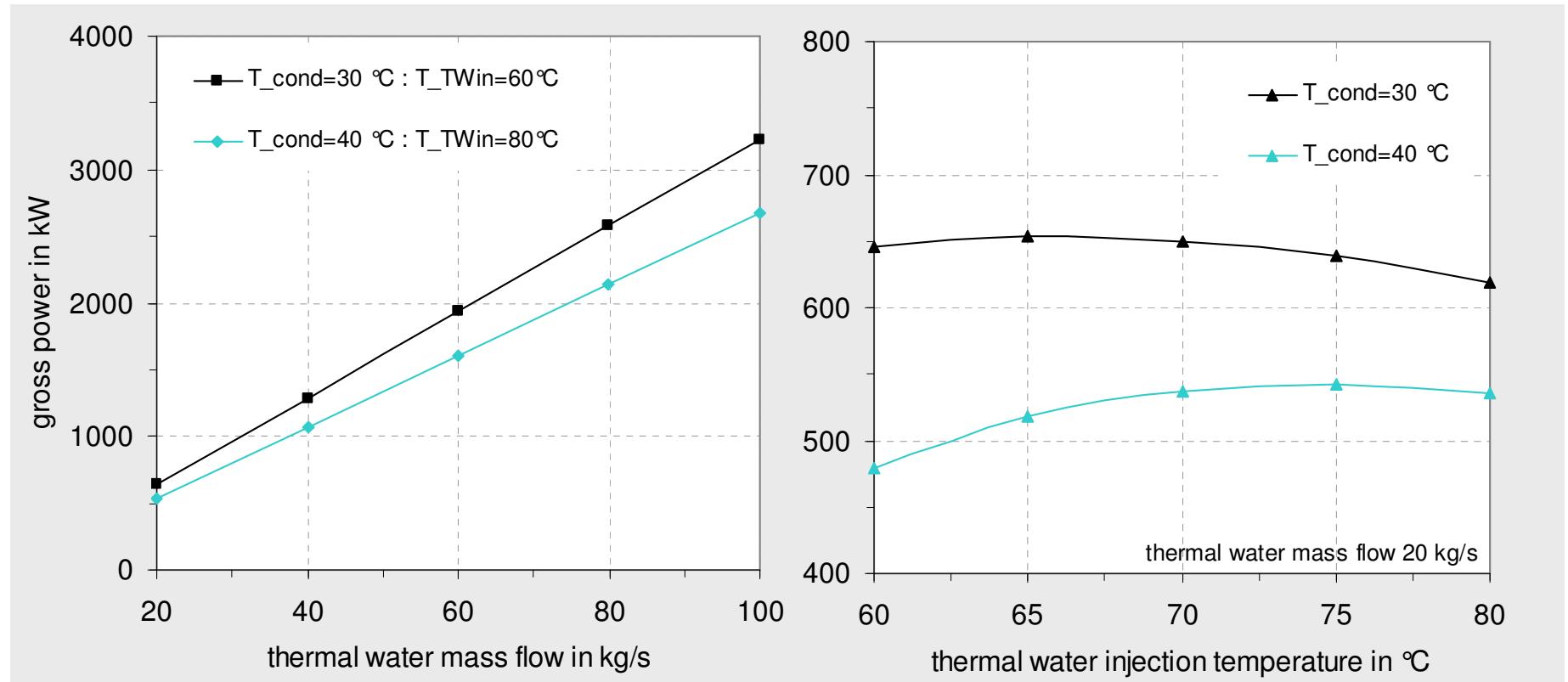
other parameters see slide 13



Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)

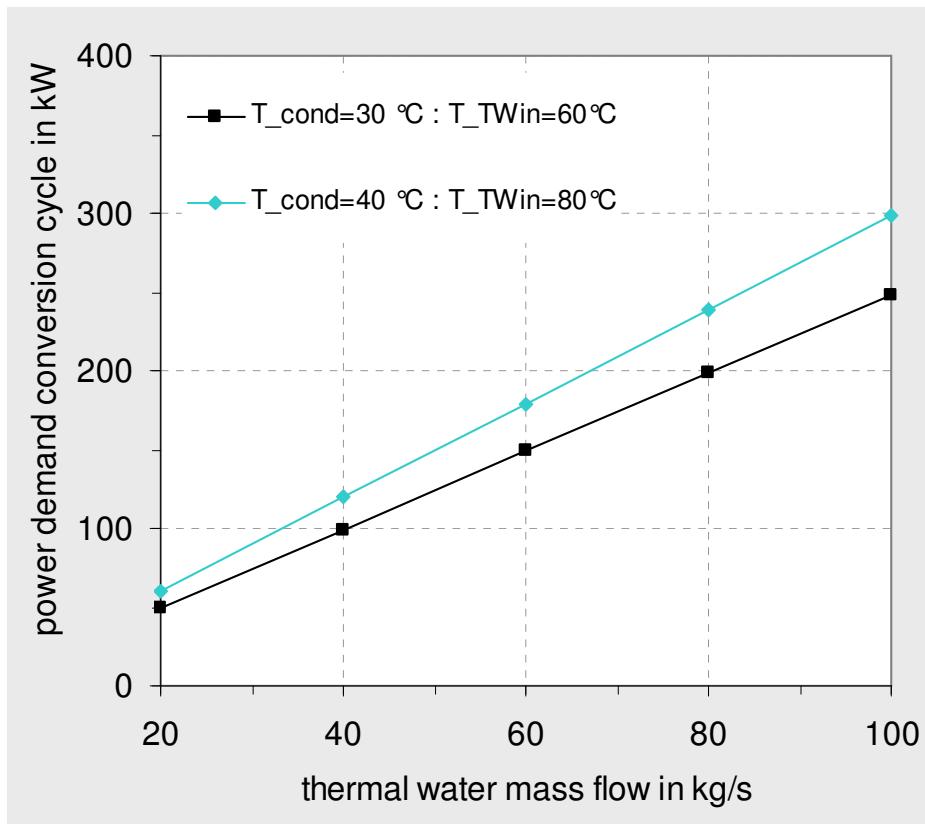


Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)

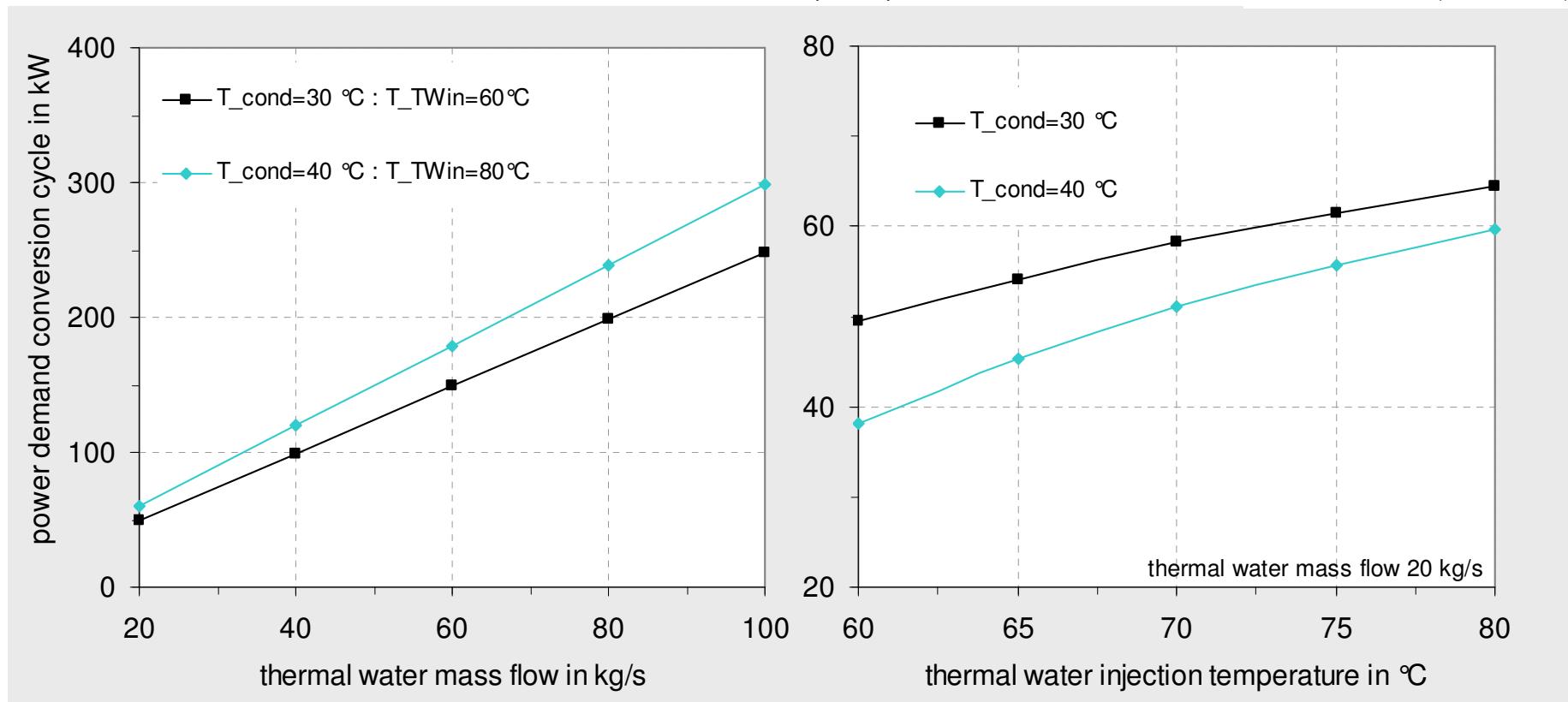


$$\text{gross power} = f(T_{cond}, T_{TW,in}) \cdot \dot{m}_{TW}$$

Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)

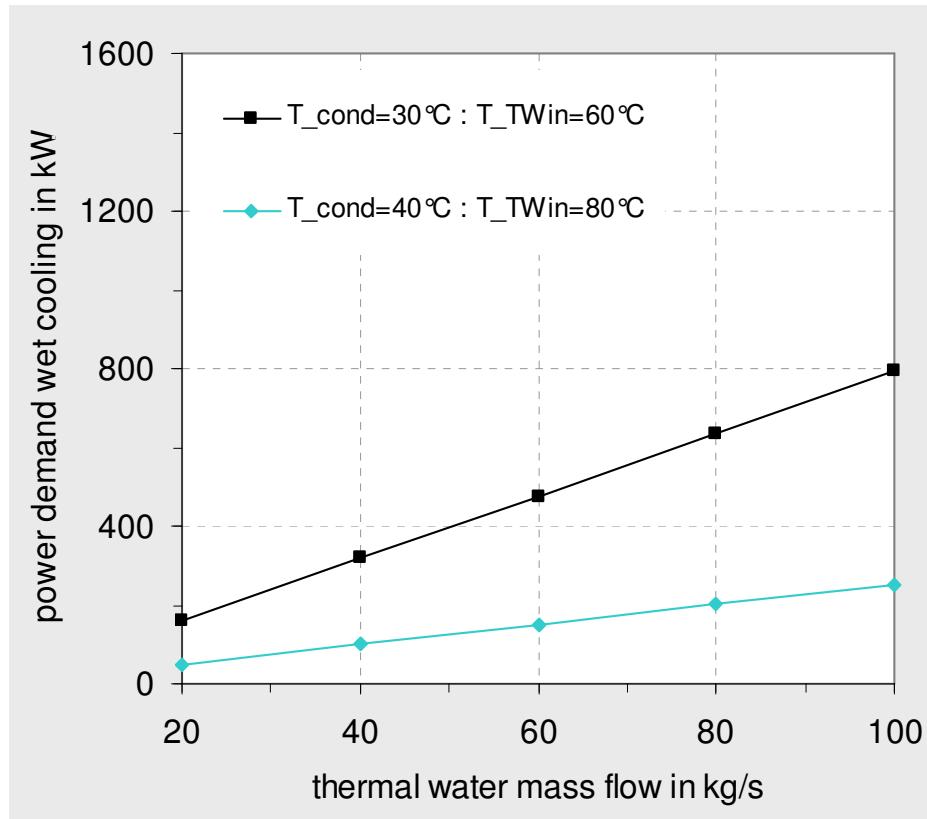


Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)



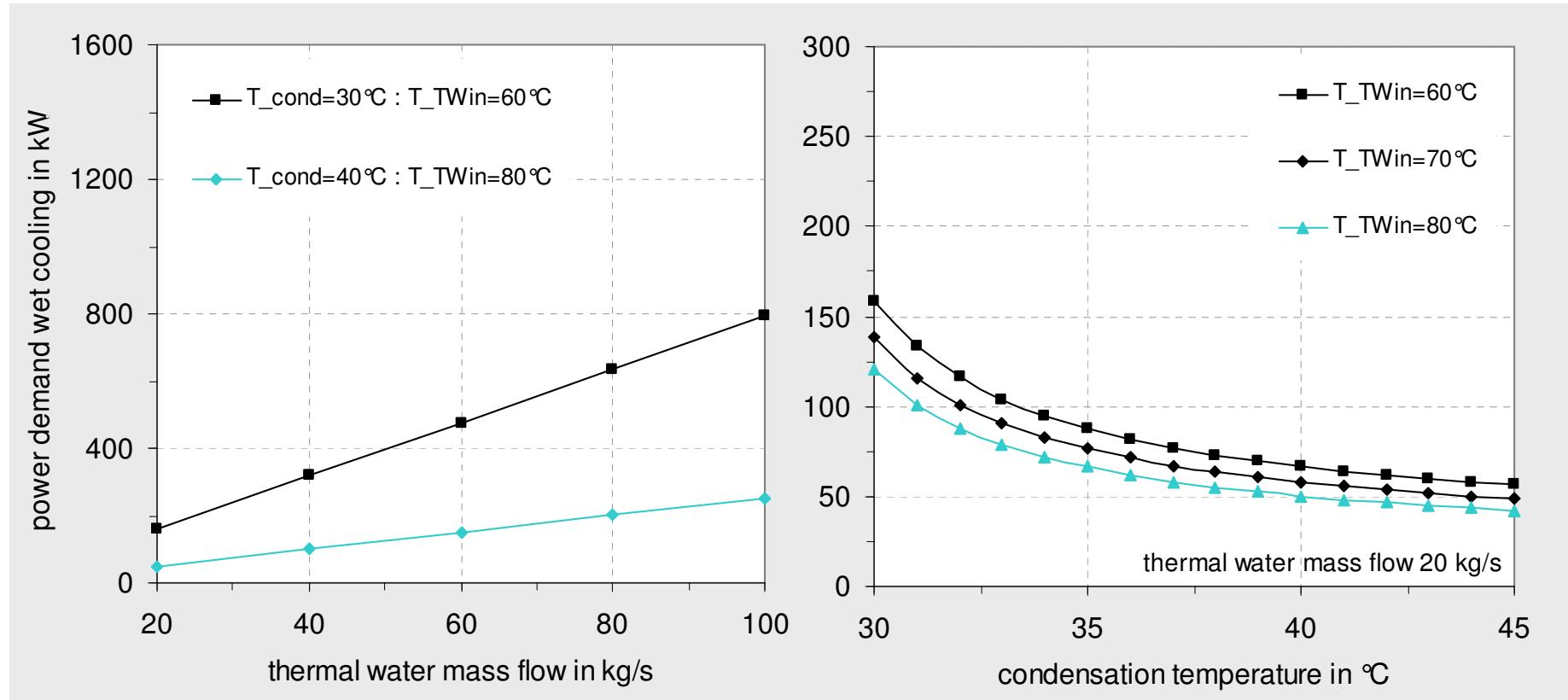
Power demand conversion cycle = $f(T_{cond}, T_{TW,in}) \cdot \dot{m}_{TW}$

Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)



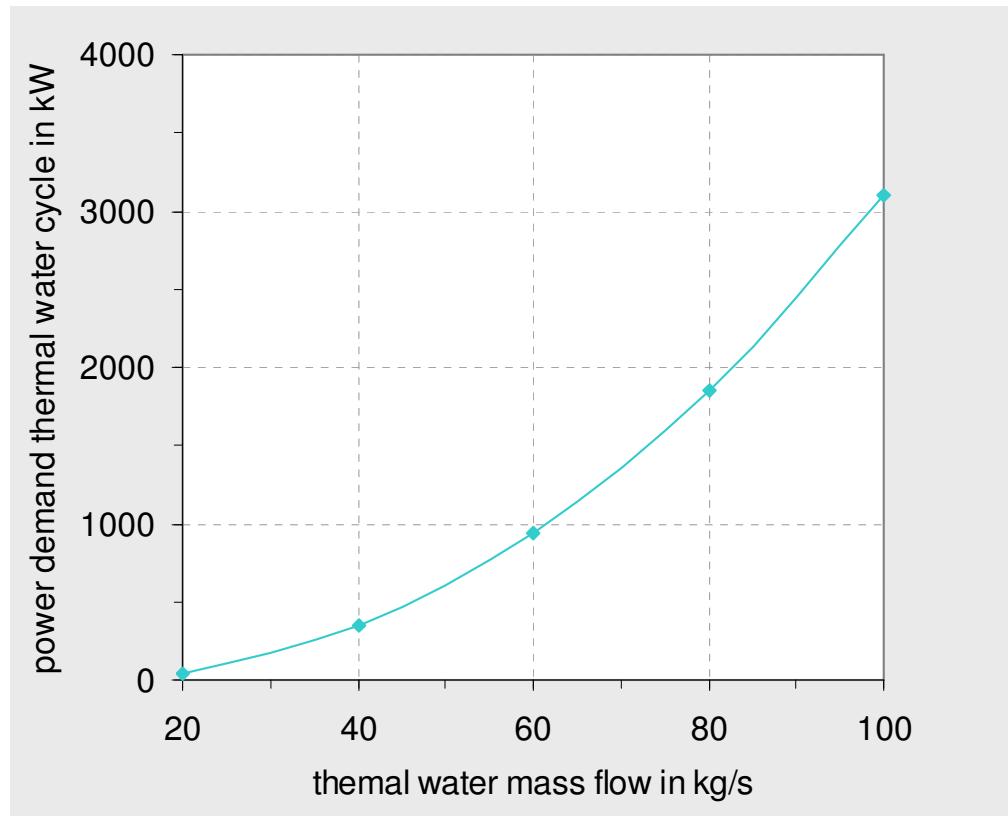
Auxiliary power characteristics Cooling cycle (wet cooling tower)

Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)

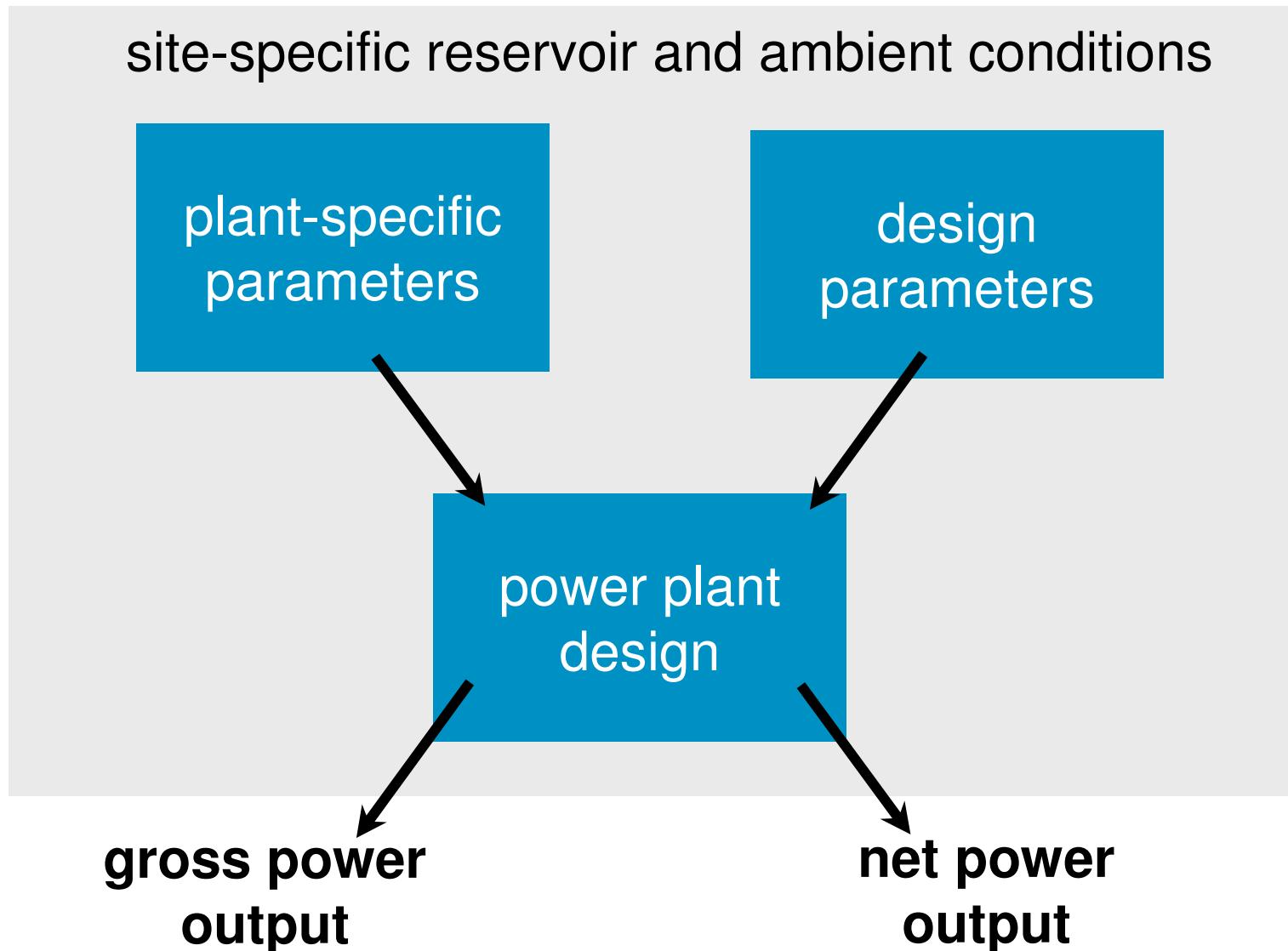


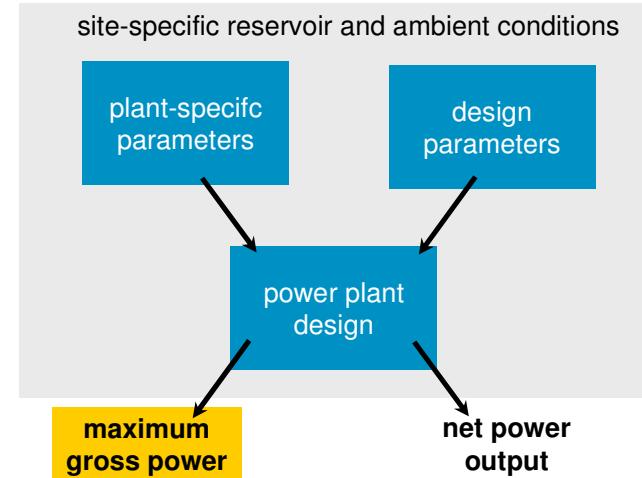
Power demand _{cooling cycle} = $f(T_{cond}) \cdot T_{TW,in} \cdot \dot{m}_{TW}$

Plant-specific parameters, reservoir and ambient conditions = const. (see slide 13)

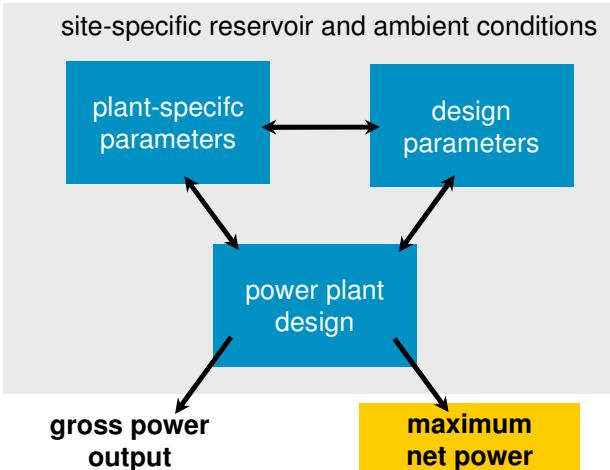


Power demand _{thermal water cycle} = $f(\dot{m}_{TW})$



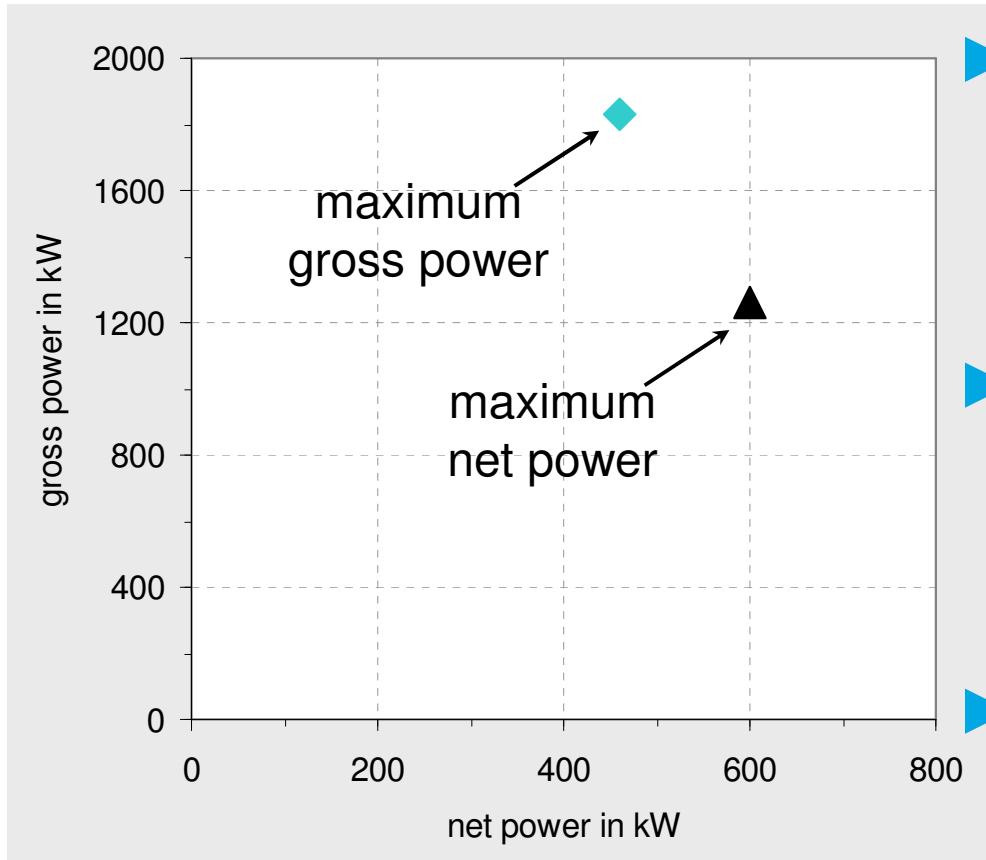


	maximum gross power (wet cooling)	maximum net power (wet cooling)
reservoir conditions	$T_{TW} = 150 \text{ }^{\circ}\text{C}$, $PI = 30 \text{ m}^3/(\text{h MPa})$, $\text{depth}_{\text{reservoir}} = 4,500 \text{ m}$	
thermal water mass flow	56 kg/s	
th. water injection temp.	66 $^{\circ}\text{C}$	
condensation temp.	30 $^{\circ}\text{C}$	
gross power	1,8 MW	
net power	460 kW	



	maximum gross power (wet cooling)	maximum net power (wet cooling)
reservoir conditions	$T_{TW} = 150 \text{ }^{\circ}\text{C}$, $PI = 30 \text{ m}^3/(\text{h MPa})$, $\text{depth}_{\text{reservoir}} = 4,500 \text{ m}$	
thermal water mass flow	56 kg/s	41 kg/s
th. water injection temp.	66 $^{\circ}\text{C}$	71 $^{\circ}\text{C}$
condensation temp.	30 $^{\circ}\text{C}$	33 $^{\circ}\text{C}$
gross power	1,8 MW	1,3 MW
net power	460 kW	600 kW

Conclusions



- ▶ Choice of \dot{m}_{TW} , $T_{TW,in}$ and T_{cond} has a decisive impact on power plant performance
- ▶ A maximum net power output can't be reached by maximising the gross power!
- ▶ Geothermal power plant design needs a holistic approach

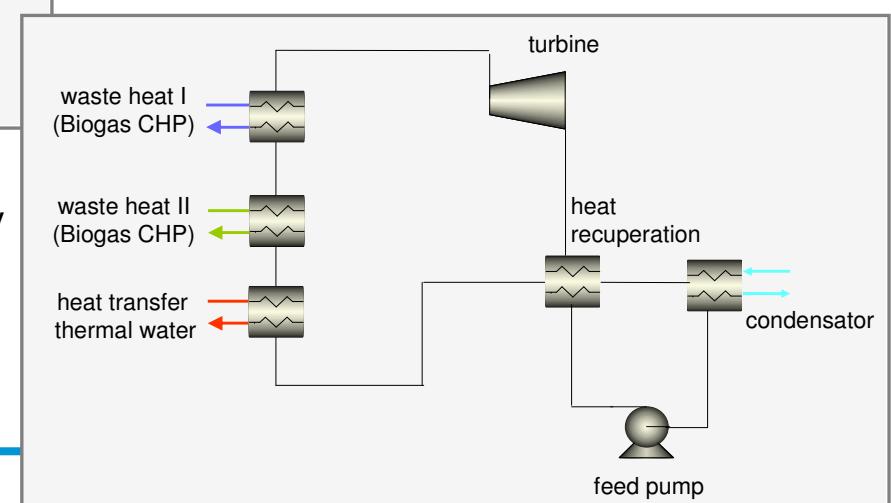
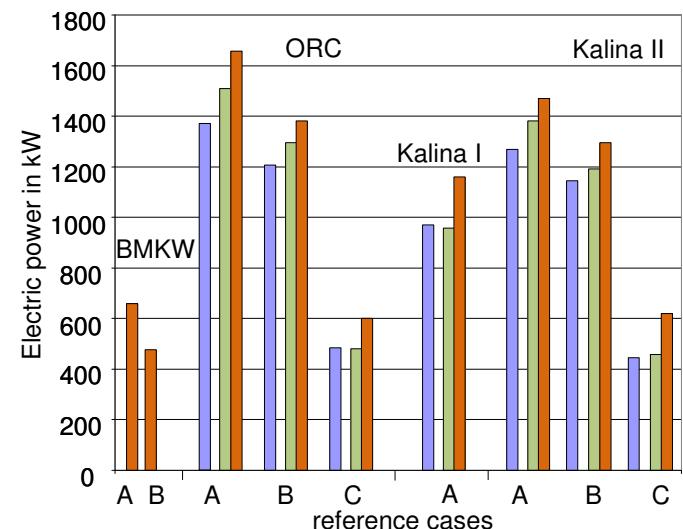
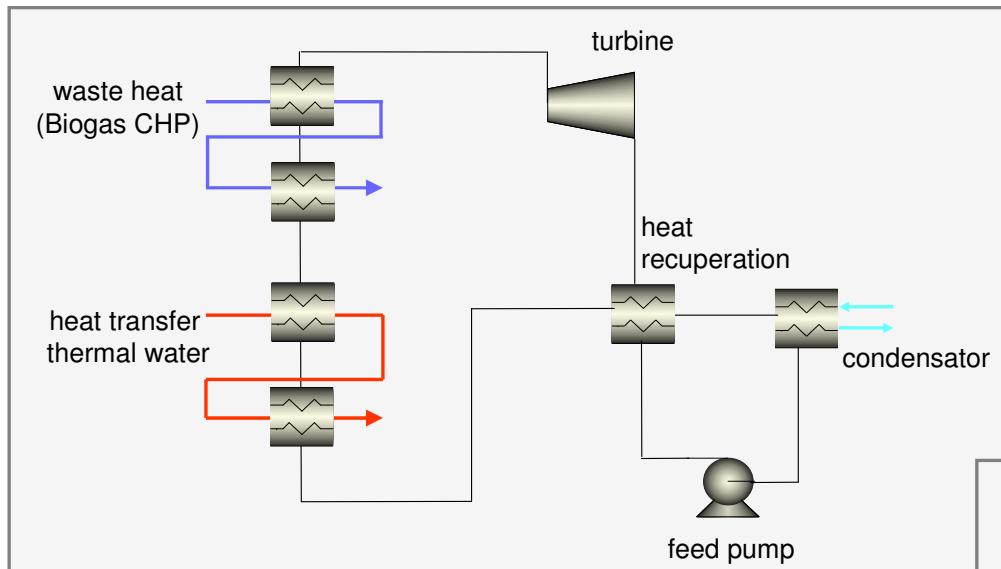
- Successful geothermal project development needs a detailed and site-specific analysis
- Further technical constraints need to be considered
- Possible combination with other energy carriers to hybrid-plants (...please have a look at the poster “The combined use of geothermal and biomass for power generation - drawbacks and opportunities –“)

The combined use of geothermal and biomass for power generation

- drawbacks and opportunities -

ENGINE Final Conference
poster session

Jan Wrobel ^a, Martin Kaltschmitt ^{a,b}



- Successful geothermal project development needs a detailed and site-specific analysis
- Further technical constraints need to be considered
- Possible combination with other energy carriers to hybrid-plants (...please have a look at the poster “The combined use of geothermal and biomass for power generation - drawbacks and opportunities –“)
- Non-technical aspects can be further limiting factors
- Successful geothermal development needs integrating, holistic planning tools

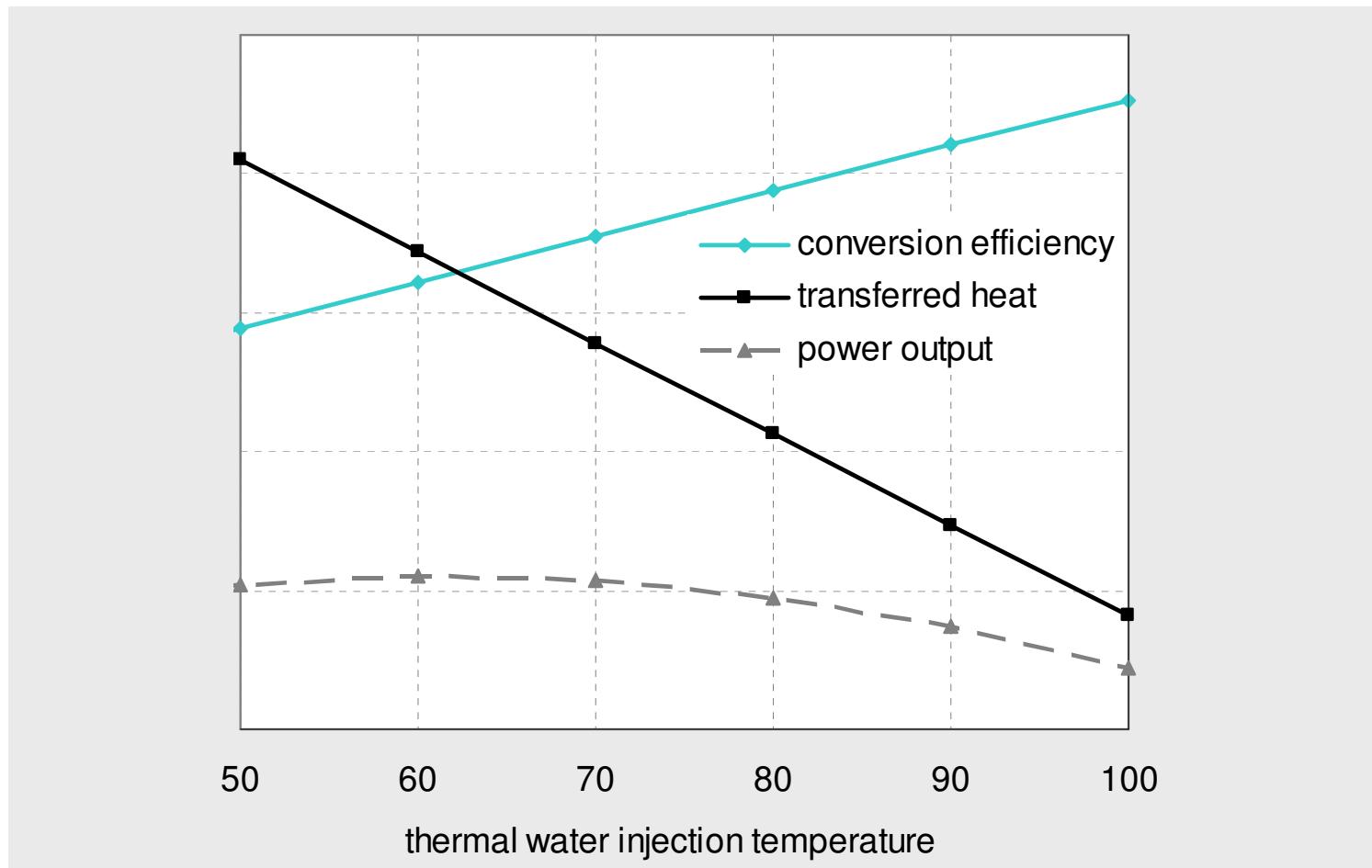
Thank you very much for your attention!

Contact:

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<http://www.gfz-potsdam.de/pb52>

	plant-specific parameters	reservoir and ambient conditions
conversion cycle	turbine isentropic efficiency 75% turbine mechanical efficiency 95% heat exchanger temp. gradients 5K heat exchanger pressure losses 0,1 bar working fluid Isobutane	
cooling cycle	<i>wet cooling:</i> water-sided pressure losses 1 bar air-sided pressure losses 0,002 bar cooling range 6K approach 3K cooling tower constant 0,8 cooling pump efficiency 80% fan efficiency 80% <i>dry cooling:</i> air-sided pressure losses 0,002 bar fan efficiency 80%	ambient temperature 20 °C relative humidity 60%
thermal water cycle	down-hole pump efficiency 60% misc. parameter see [Legarth, 2005]	thermal water temperature 150 °C reservoir depth 4,500 m thermal water heat capacity 3,5 kJ/(kg K) thermal water density 1,147 kg/m ³ productivity-/injectivity index 30 m ³ /(h MPa)

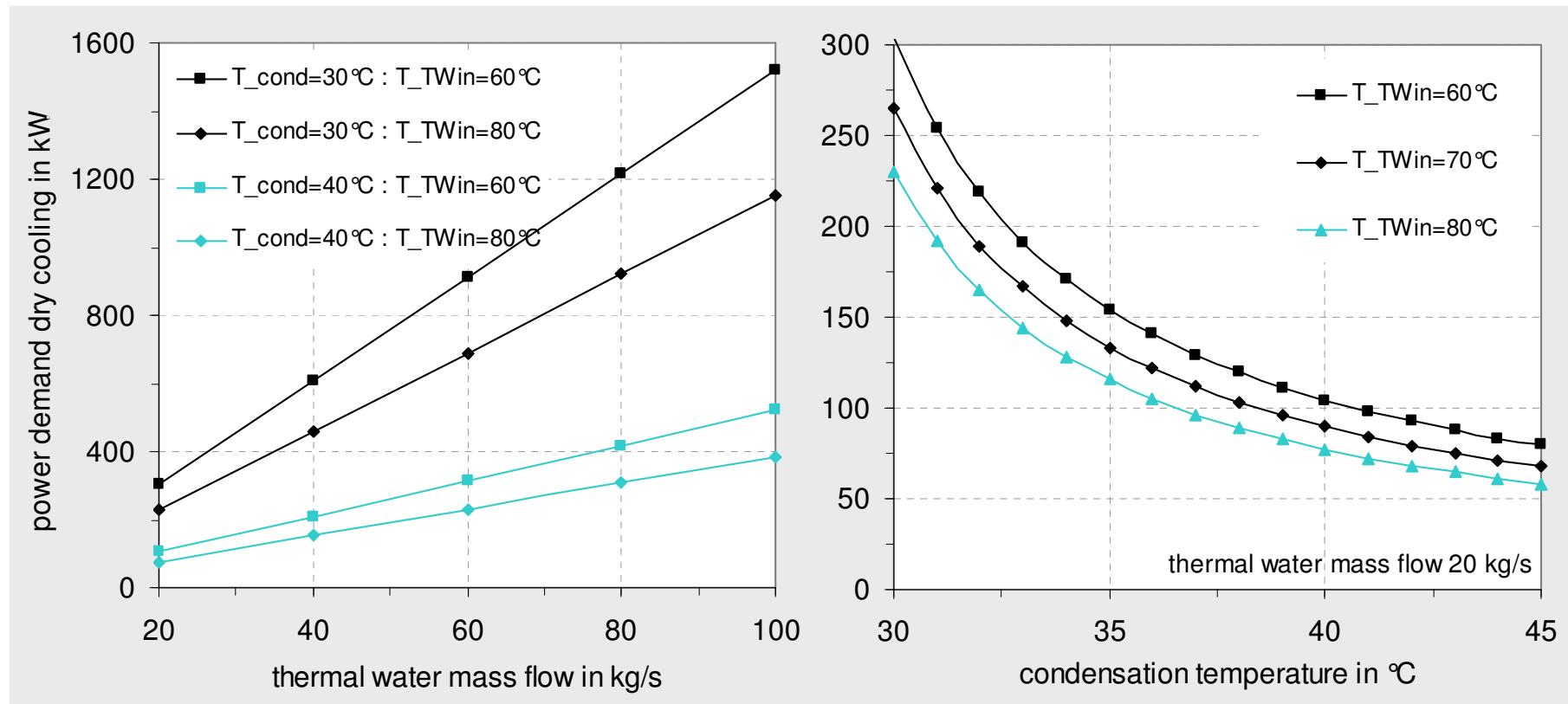
Exemplary run of power output against thermal water injection temperature



Power output = transferred heat × conversion efficiency

Auxiliary power characteristics Cooling cycle (dry condensation)

Plant-specific parameter, reservoir and ambient conditions = const. (see slide 13)



Power demand _{cooling cycle} = $f(T_{cond}) \cdot T_{TW,in} \cdot \dot{m}_{TW}$

	maximum gross power (wet cooling)	maximum gross power (dry cooling)	maximum net power (wet cooling)	maximum net power (dry cooling)
reservoir conditions	$T_{TW} = 150 \text{ }^{\circ}\text{C}$, $PI = 30 \text{ m}^3/(\text{h MPa})$, $\text{depth}_{\text{reservoir}} = 4,500 \text{ m}$			
thermal water mass flow	56 kg/s	56 kg/s	41 kg/s	37 kg/s
th. water injection temp.	66 $^{\circ}\text{C}$	66 $^{\circ}\text{C}$	71 $^{\circ}\text{C}$	73 $^{\circ}\text{C}$
condensation temp.	30 $^{\circ}\text{C}$	30 $^{\circ}\text{C}$	33 $^{\circ}\text{C}$	36 $^{\circ}\text{C}$
gross power	1,8 MW	1,8 MW	1,3 MW	1,1 MW
net power	460 kW	100 kW	600 kW	485 kW