

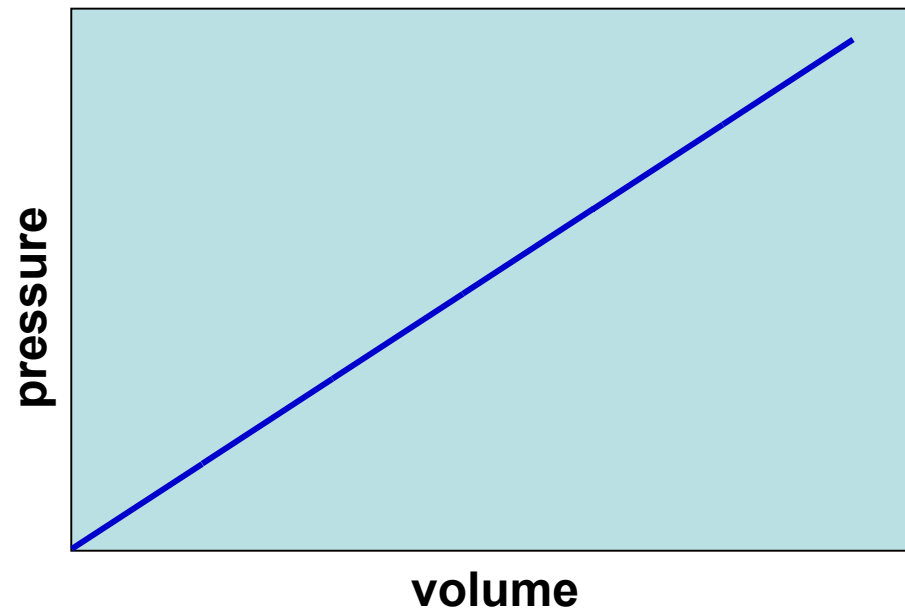
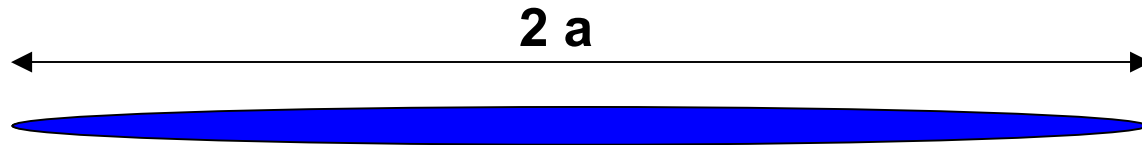
Figure 5-2. Cross-sectional view of a propagating fracture.

Review of Hydraulic Stimulation Technology

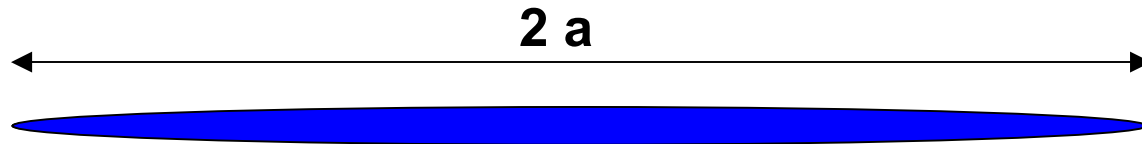
R. Jung, F. Rummel

ENGINE Workshop 3
Ittingen 29./30.06.2006

Mechanical properties of fractures



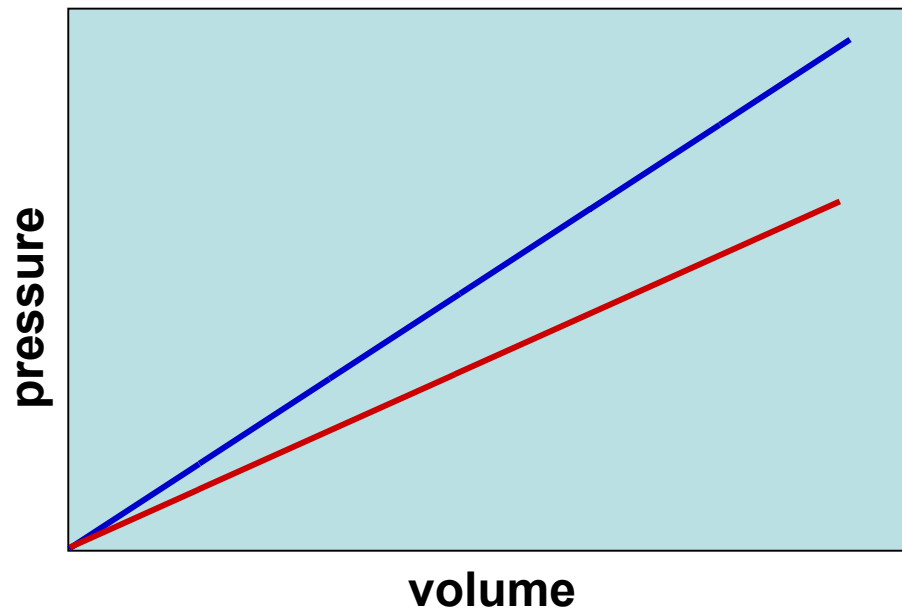
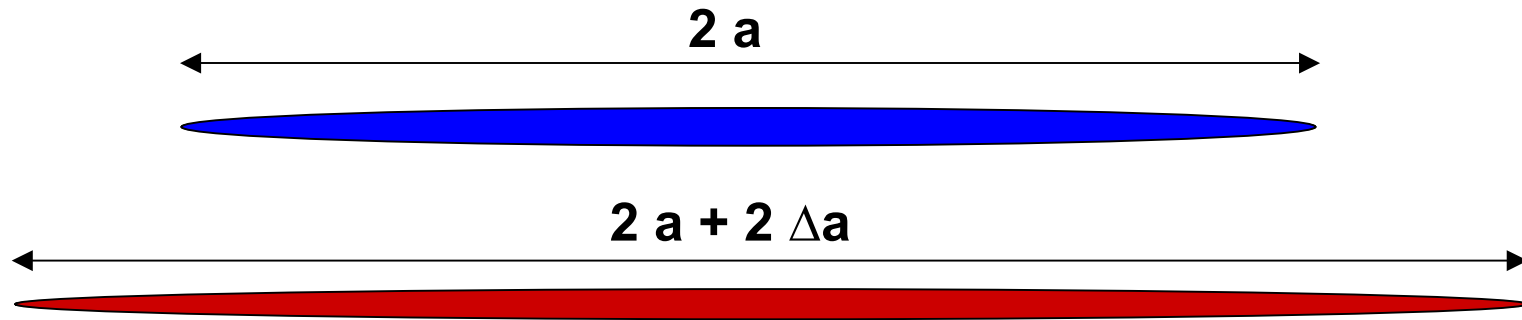
Mechanical properties of fractures



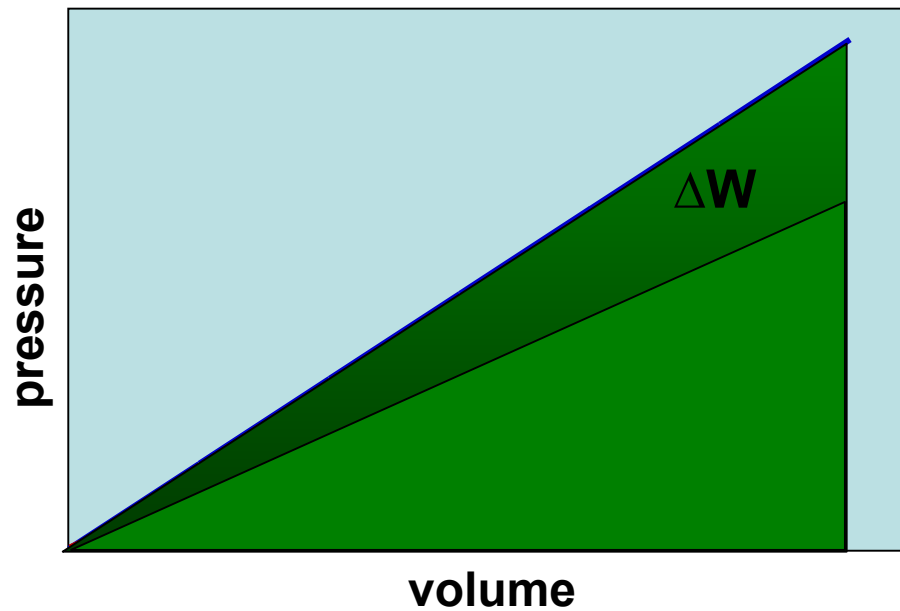
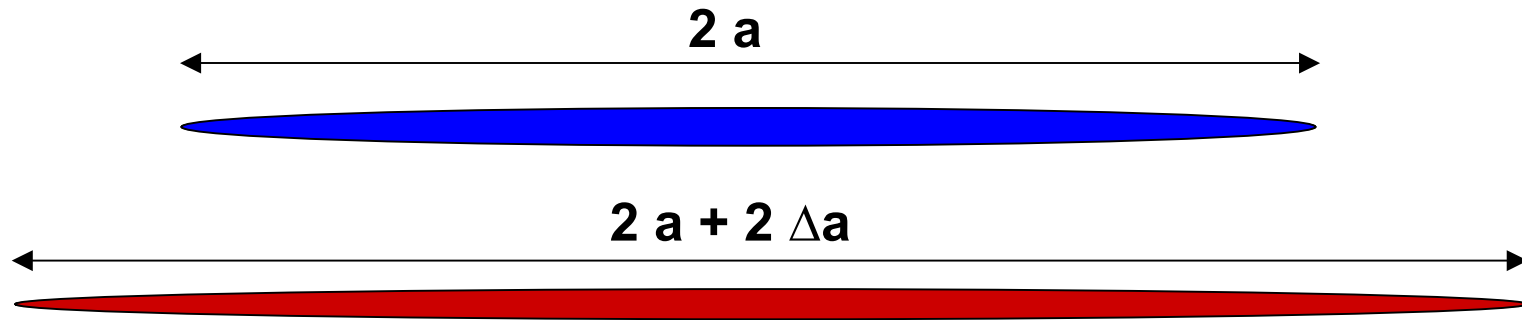
$2a$	dw/dp	dV/dp
[m]	[mm/bar]	[m ³ /bar]
1	0.003	$3 \cdot 10^{-6}$
10	0.03	0.003
100	0.3	3
1000	3	3000
in contact	0.001-0.01	

$$E = 50 \text{ GPa}$$

Mechanical properties of fractures



Fracture propagation



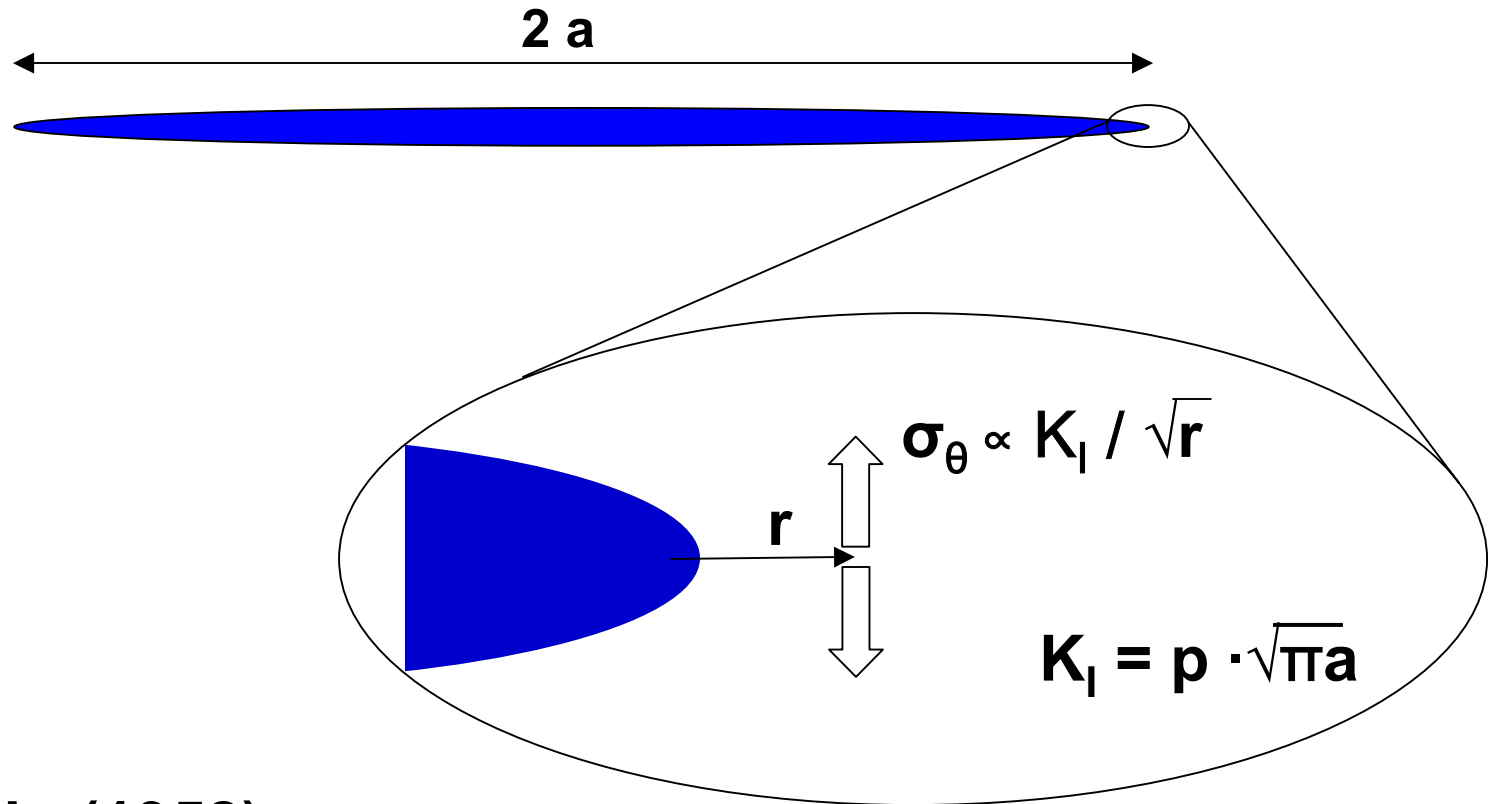
Griffith (1921)

$$\Delta W \geq 2 \Delta a \cdot \gamma$$

γ : surface energy

$$\gamma = 10 - 100 \text{ J/m}^2$$

Fracture propagation



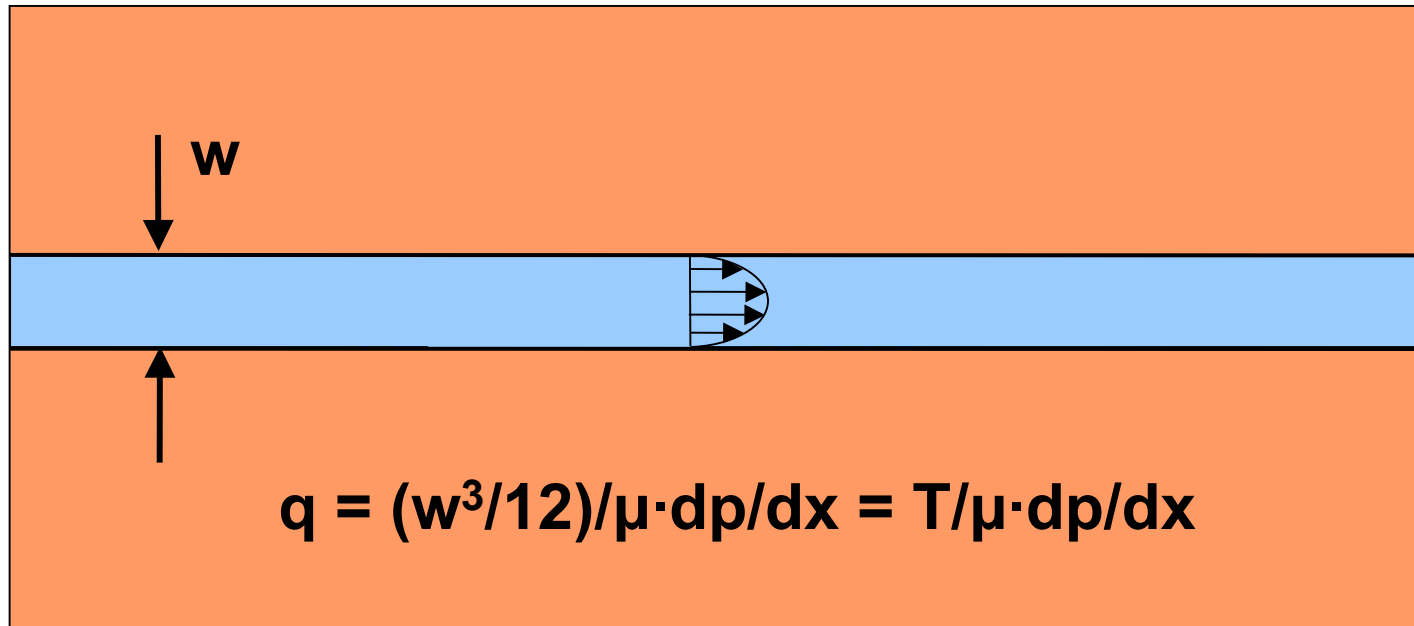
Irvin (1958)

$$K_I = K_{IC}$$

K_{IC} : fracture toughness

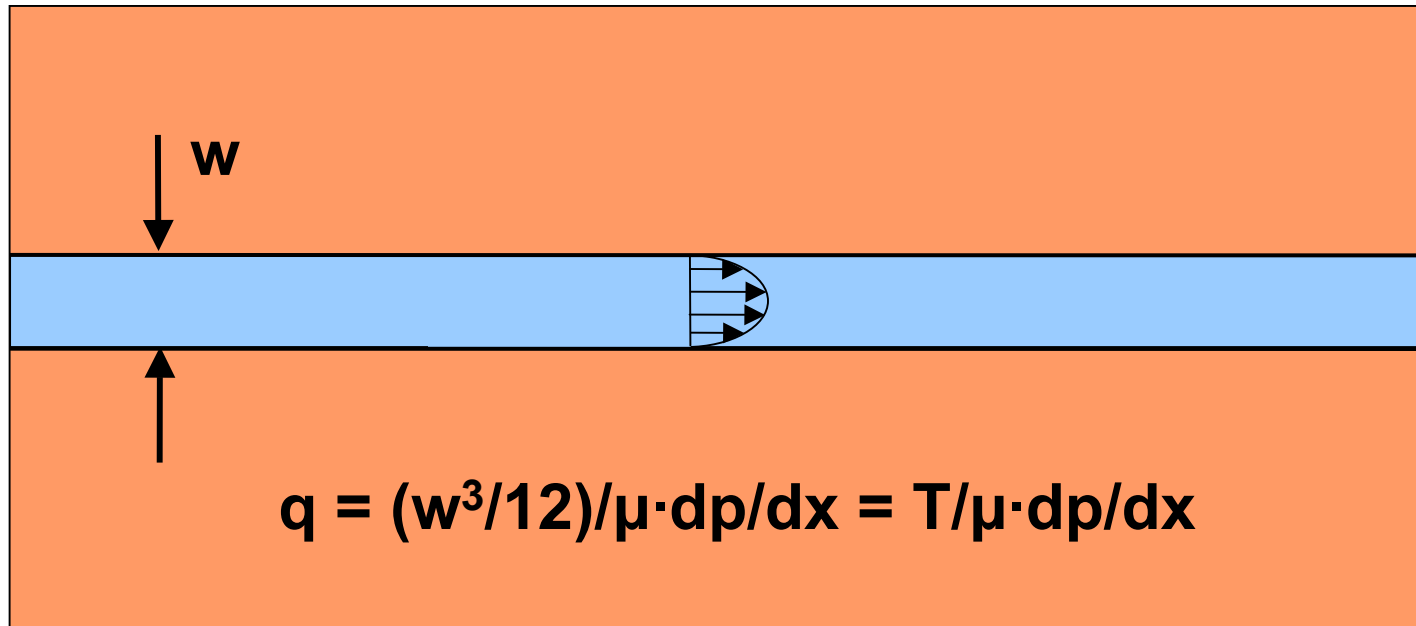
$$K_{IC} = 1 \text{ MPa} \cdot \text{m}^{1/2}$$

fluid flow in fractures



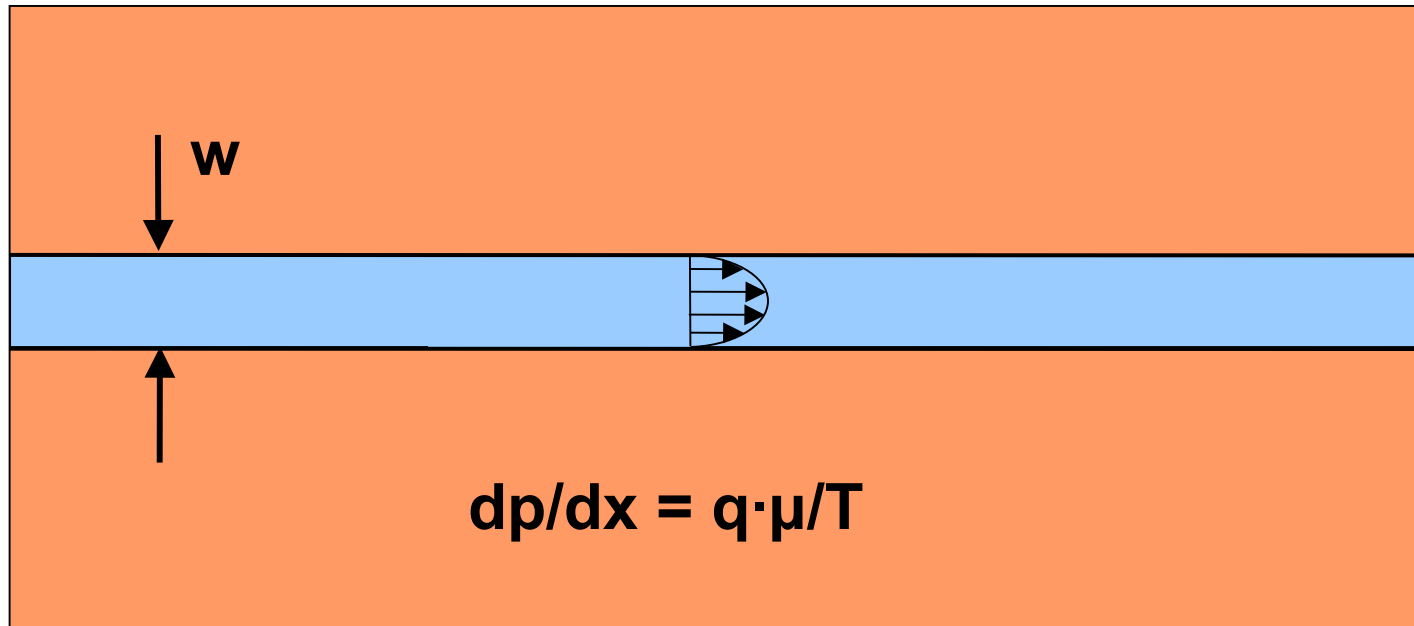
T : fracture transmissibility
 μ : viscosity

fluid flow in fractures



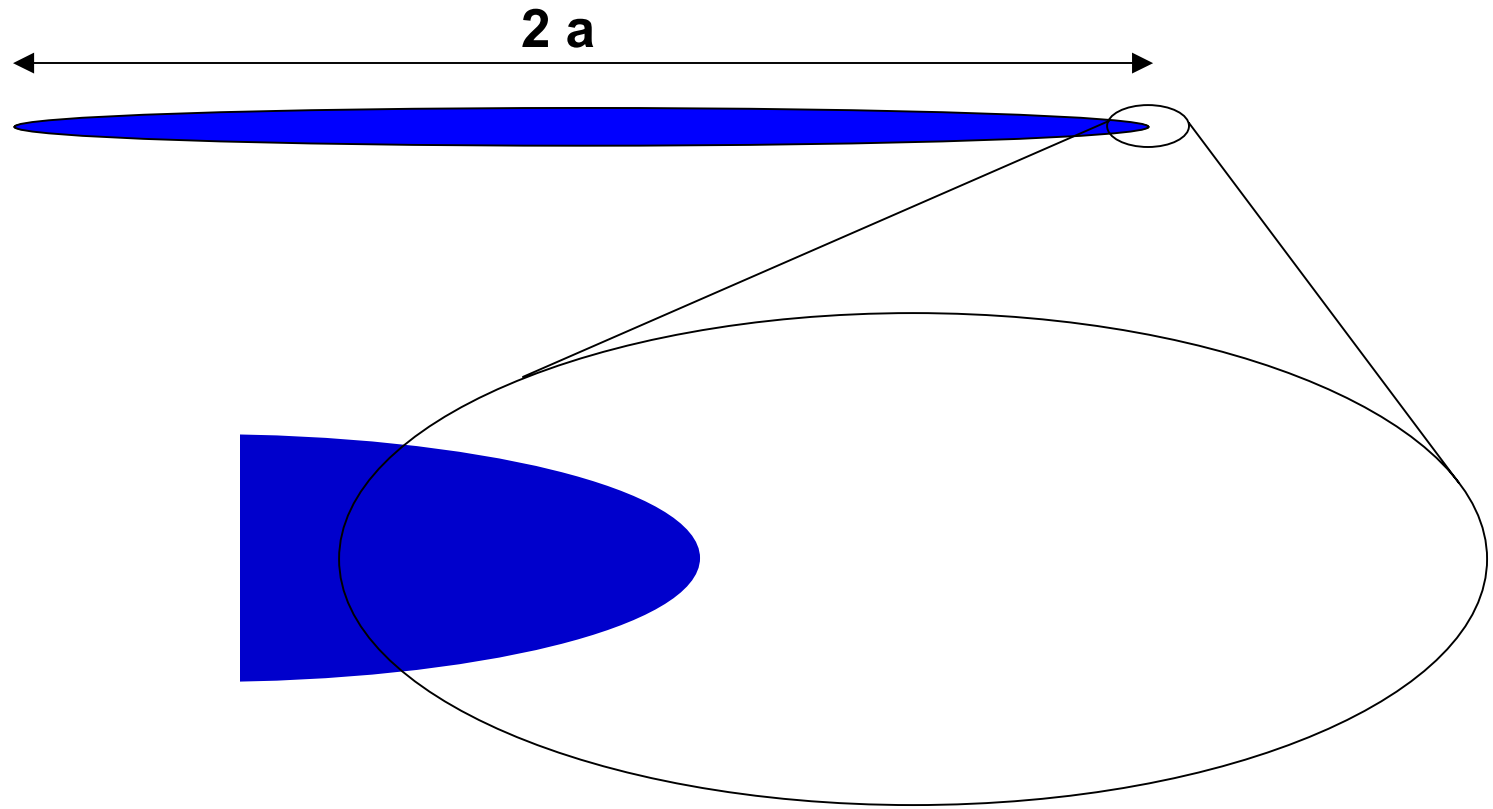
w	T	T
[mm]	[m ³]	[D·m]
0.01	10 ⁻¹⁶	10 ⁻⁴
0.1	10 ⁻¹³	0,1
1	10 ⁻¹⁰	100
10	10 ⁻⁷	10 ⁵
Porous aquifer	10 ⁻¹¹	10

fluid flow in fractures



w	q	dp/dx
[mm]	[l/(s·m)]	[bar/m]
0.01	1	10^5
0.1	1	100
1	1	0.1
10	1	10^{-4}

fluid flow in fractures



High gradients at the fracture tip

Hydrodynamic fracture models

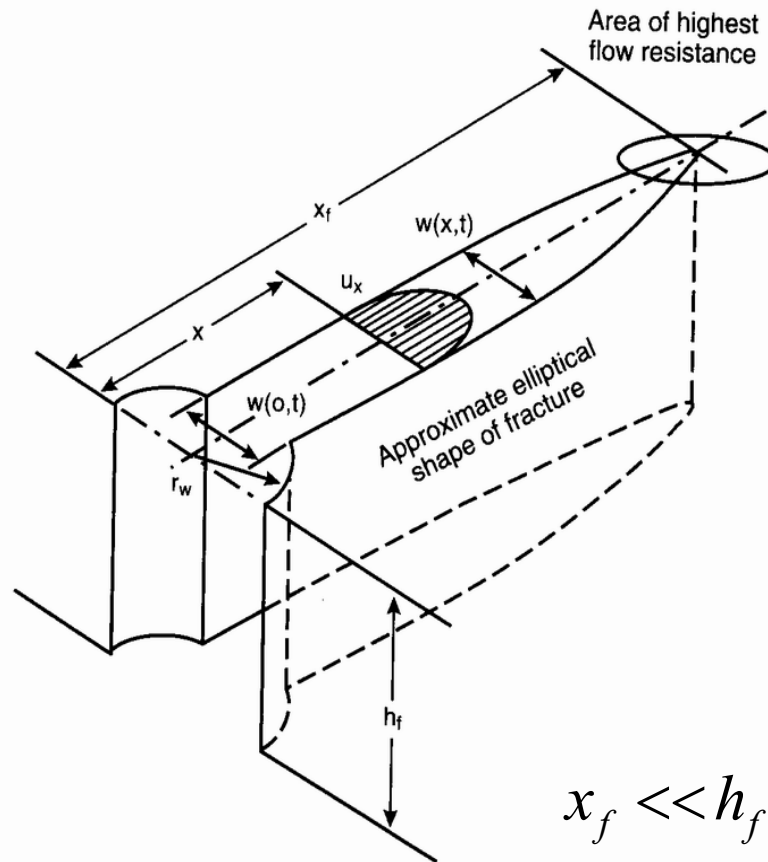


Figure 16-8

Khristianovich, Zheltov, Geertsma, de Klerk (KGD)
Model Geometry

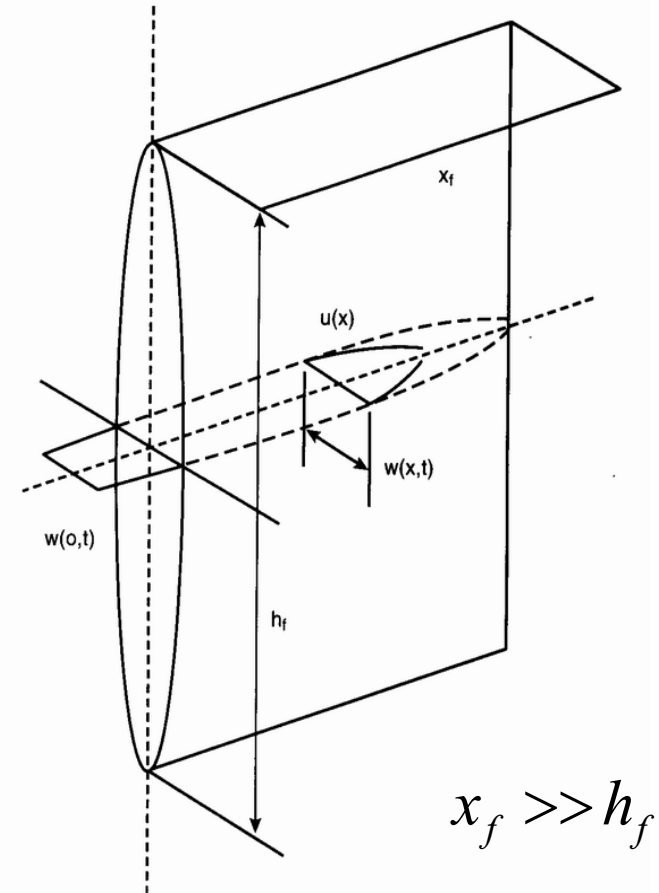


Figure 16-7

Perkins, Kern, and Nordgren (PKN)
Model Geometry

Hydrodynamic fracture models

KGD fracture model (1955, 1969)

$$\bar{w} = 2,27 \cdot \left[\frac{q_i \cdot \mu \cdot (1-\nu) \cdot x_f^2}{G \cdot h_f} \right]^{1/4} \left(\frac{\pi}{4} \right)$$

- G = elastic shear modulus, Pa $G = \frac{E}{2 \cdot (1+\nu)}$
 q_i = injection rate, m³/s
 μ = apparent viscosity, Pa·s
 E = Young's modulus, Pa
 ν = Poisson's ratio
 x_f = fracture half length, m
 h_f = Fracture height, m

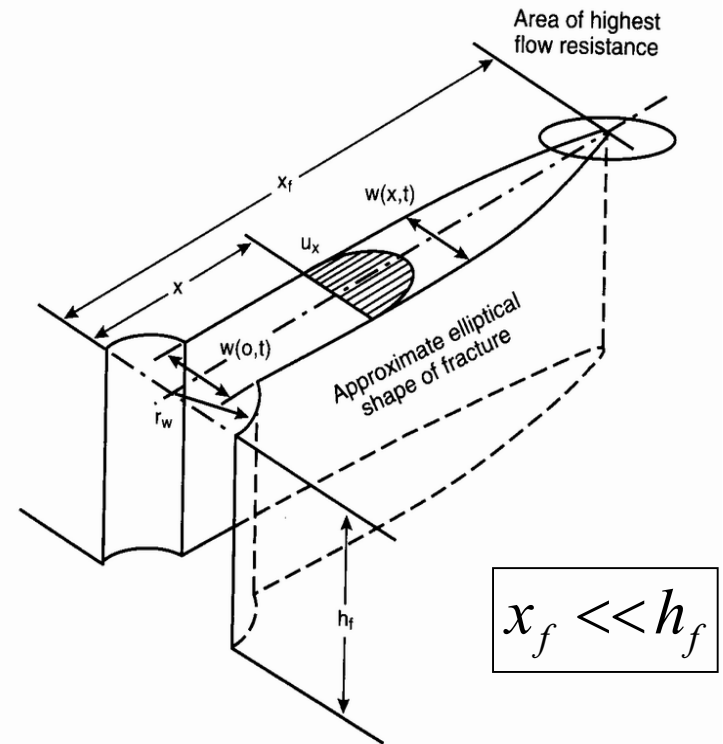
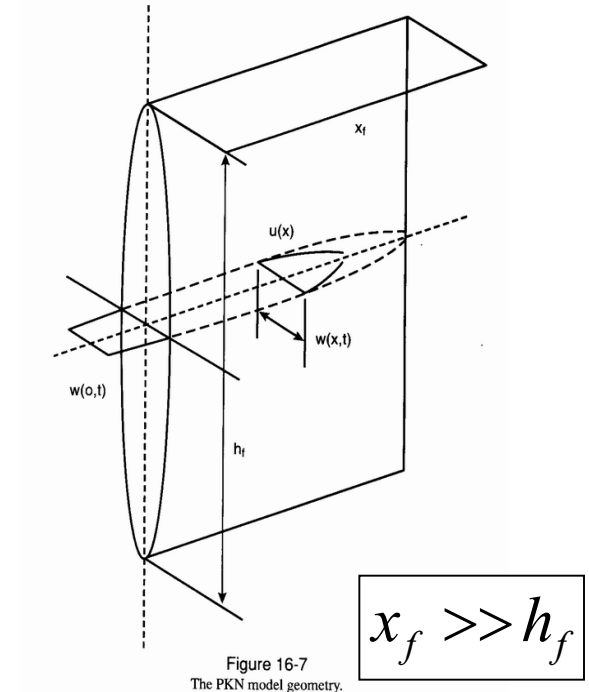


Figure 16-8
The KGD model geometry.

Hydrodynamic fracture models

PKN fracture model

$$\bar{w} = 2,31 \cdot \left[\frac{q_i \cdot \mu \cdot (1 - \nu) \cdot x_f}{G} \right]^{1/4} \left(\frac{\pi}{4} \cdot \gamma \right)$$



G = elastic shear modulus,
 q_i = injection rate
 μ = apparent viscosity
 E = Young's modulus (10⁷ - 2x10⁵ psi)
 ν = Poisson's ratio (0,15 - 0,4)
 x_f = fracture half length
 γ = geometry factor app. 0,75

$$G = \frac{E}{2 \cdot (1 + \nu)}$$

q_i = injection rate, bpm
 μ = apparent viscosity, cp
 G = elastic shear modulus, psi
 x_f = fracture half length, ft

Hydrodynamic fracture models

Comparison with static fracture models

2a	Griffith	KDG
[m]	w_c , [mm]	w_c , [mm]
1	0.025	0.4
10	0.075	1.2
100	0.25	4
1000	0.75	12

$q = 1 \text{ l}/(\text{s}\cdot\text{m})$ water

Fluid losses

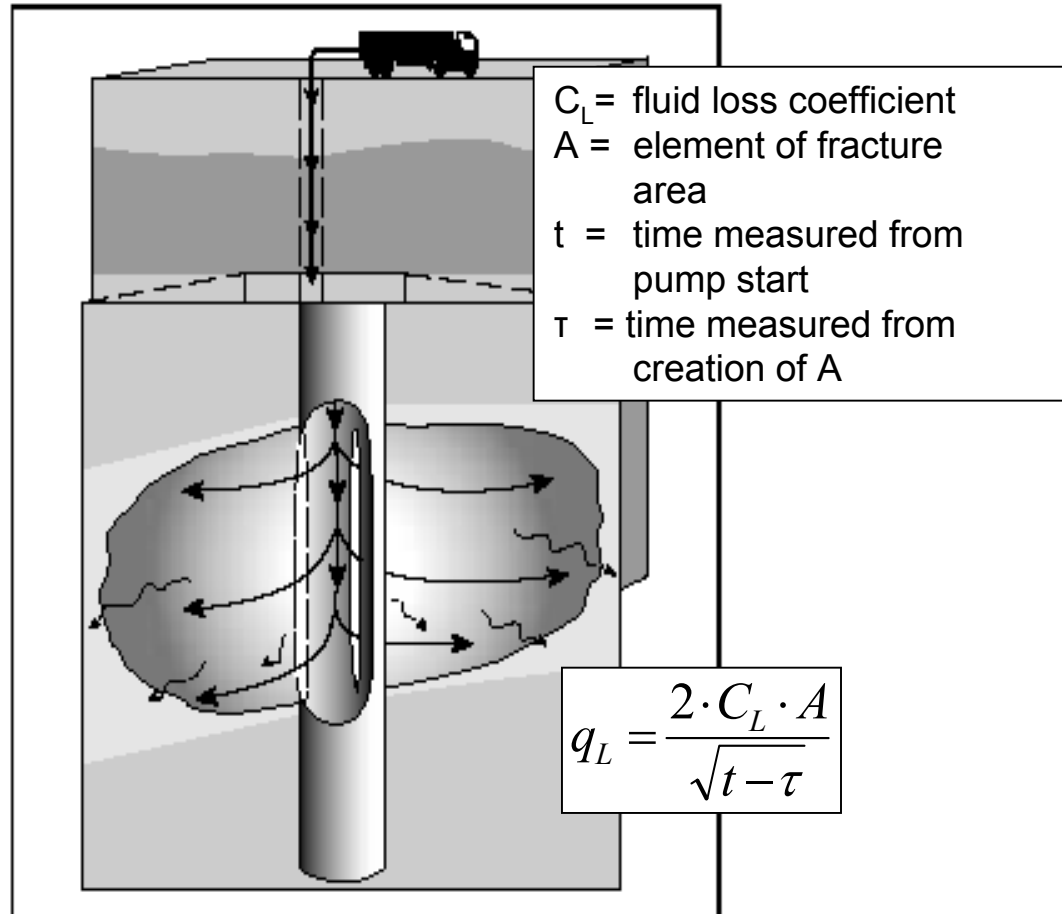


Figure 5-2. Cross-sectional view of a propagating fracture.

Fluid losses

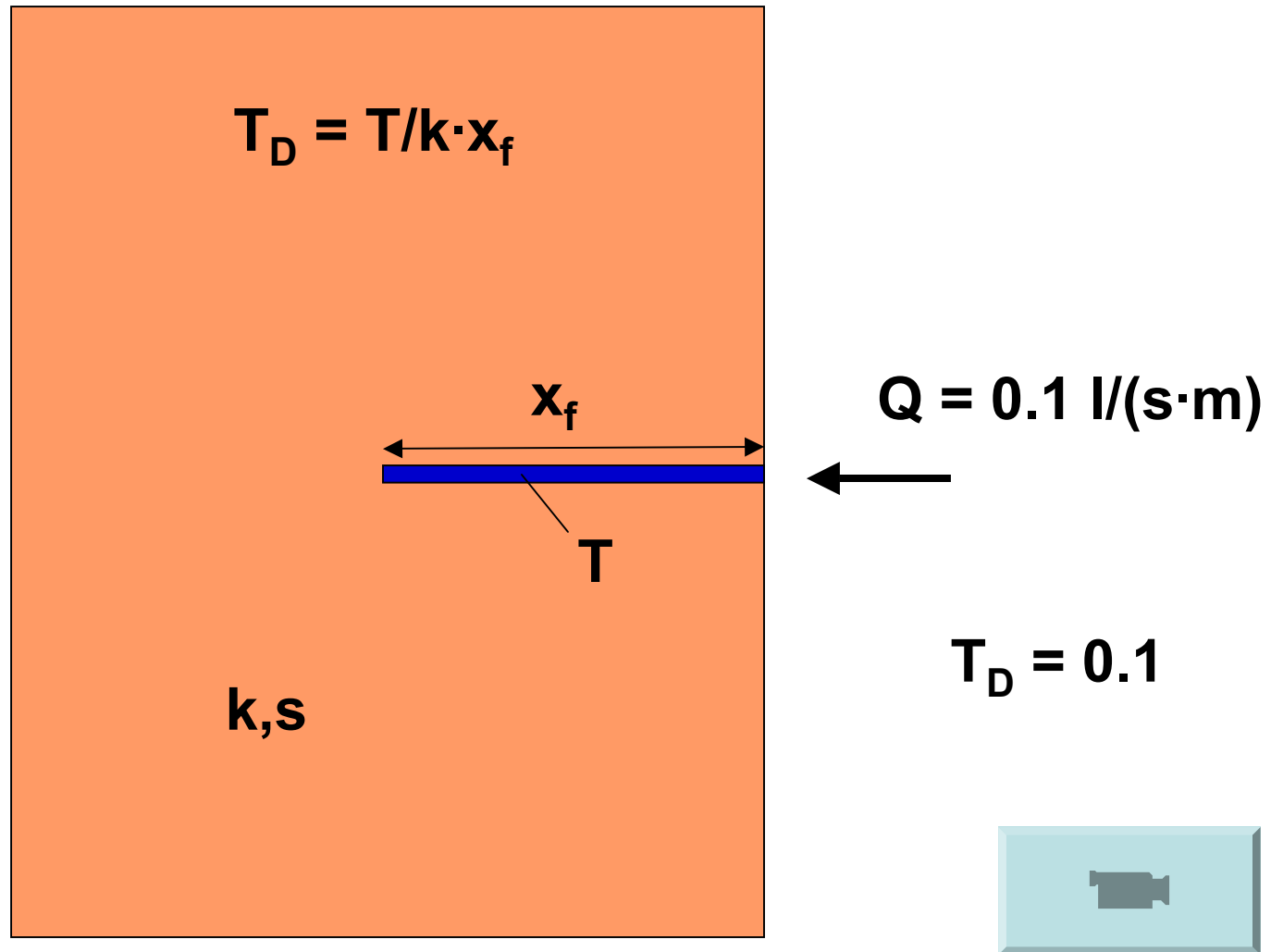
Volume injected = created fracture volume + fluid leak off

$$V_i = V_f + V_L$$

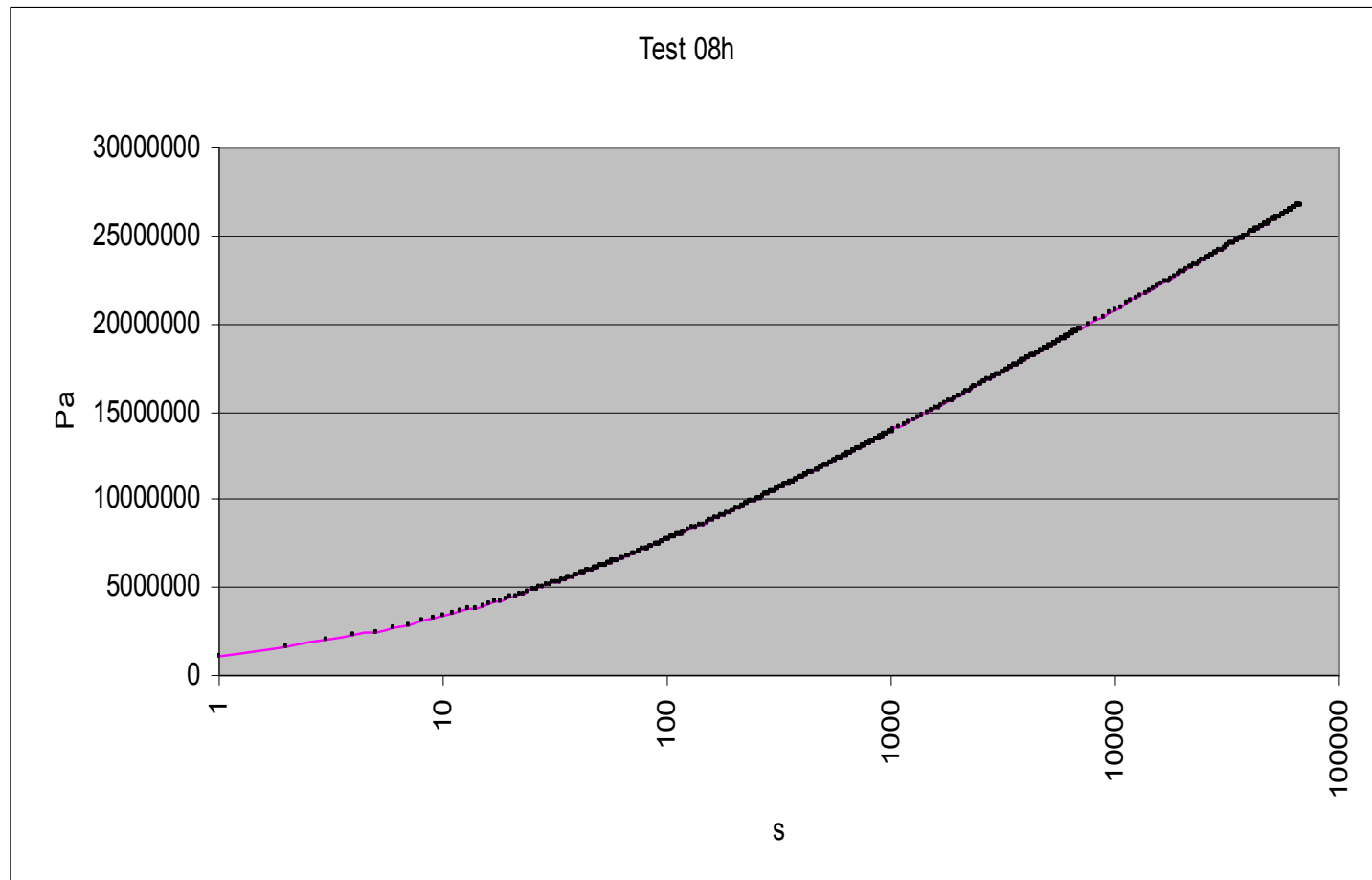
$$q_i \cdot t_i = A_f \cdot \bar{w} + K_L \cdot C_L \cdot (2 \cdot A_f) \cdot r_p \cdot \sqrt{t_i}$$

- q_i = injection rate
- t_i = injection time
- A_f = fracture area
- \bar{w} = average fracture width
- C_L = leakoff coefficient
- r_p = ratio of net to fracture height
- $K_L = \frac{1}{2} \cdot \left[\frac{8}{3} \eta + \pi \cdot (1 - \eta) \right]$ (Nolte)
- $\eta = \text{fluid efficiency} = \frac{V_f}{V_i}$
- V_{pad} = pad volume not carrying proppants

post frac tests

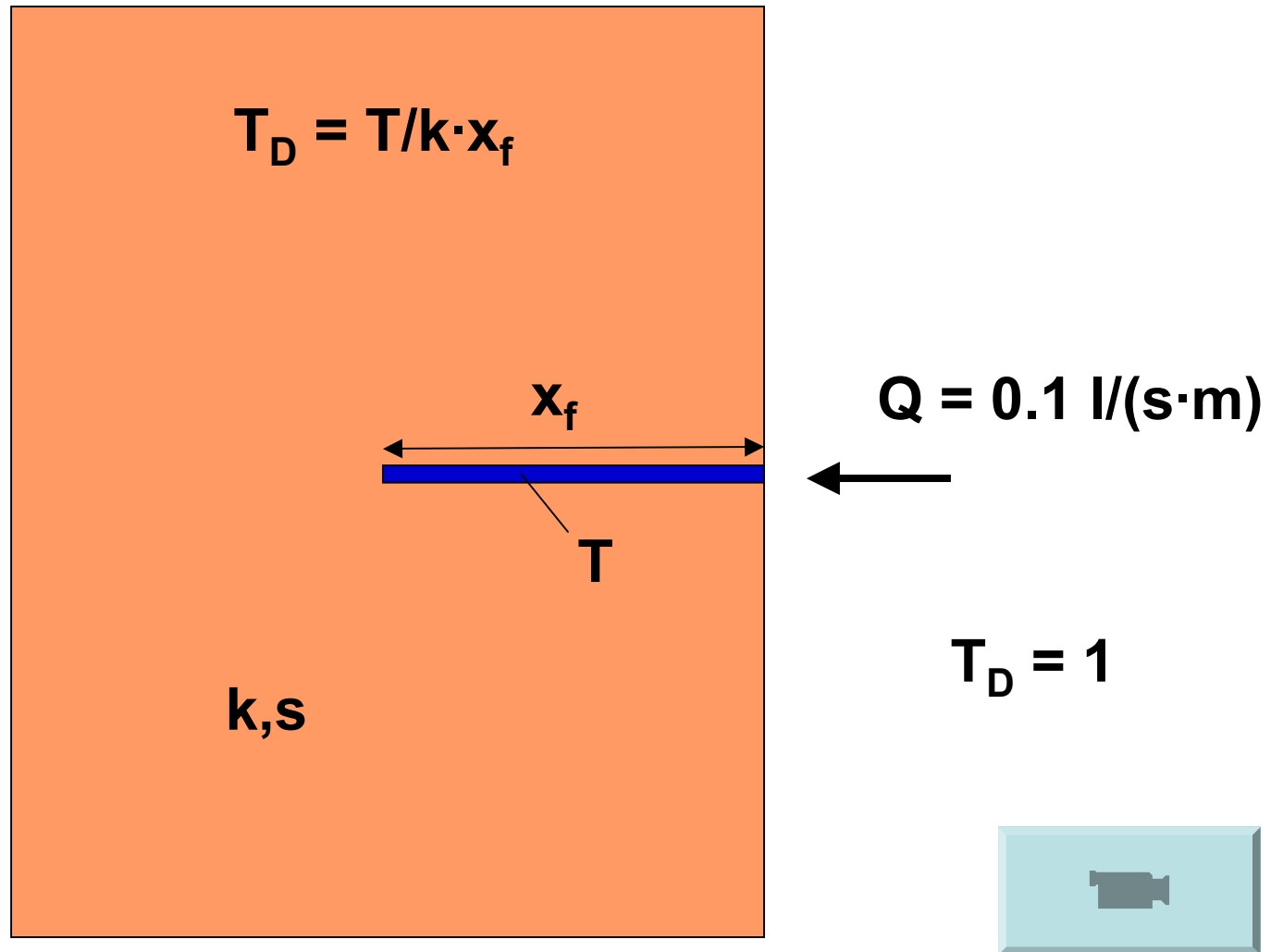


post frac tests

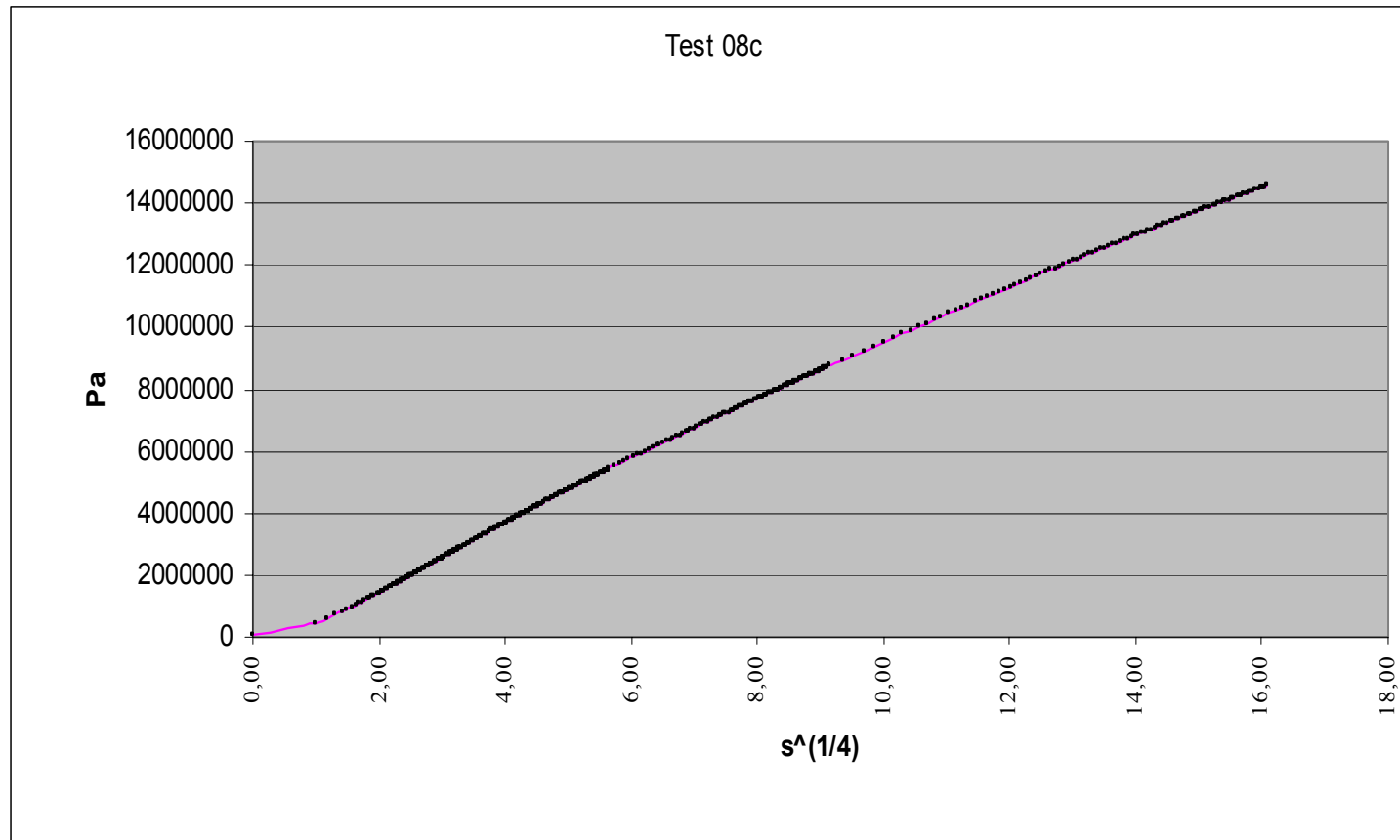


$$T_D = 0.1$$

post frac tests

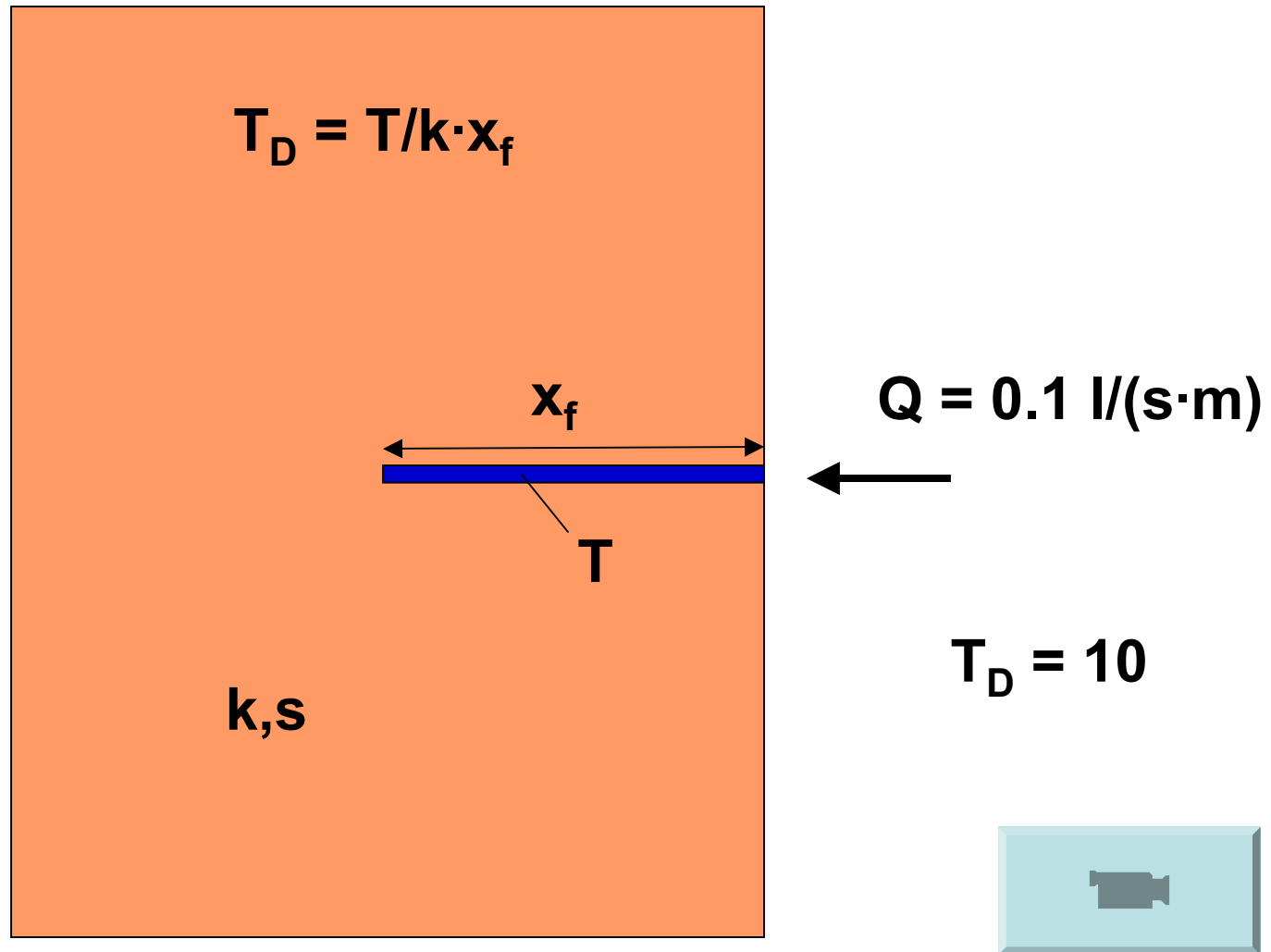


post frac tests

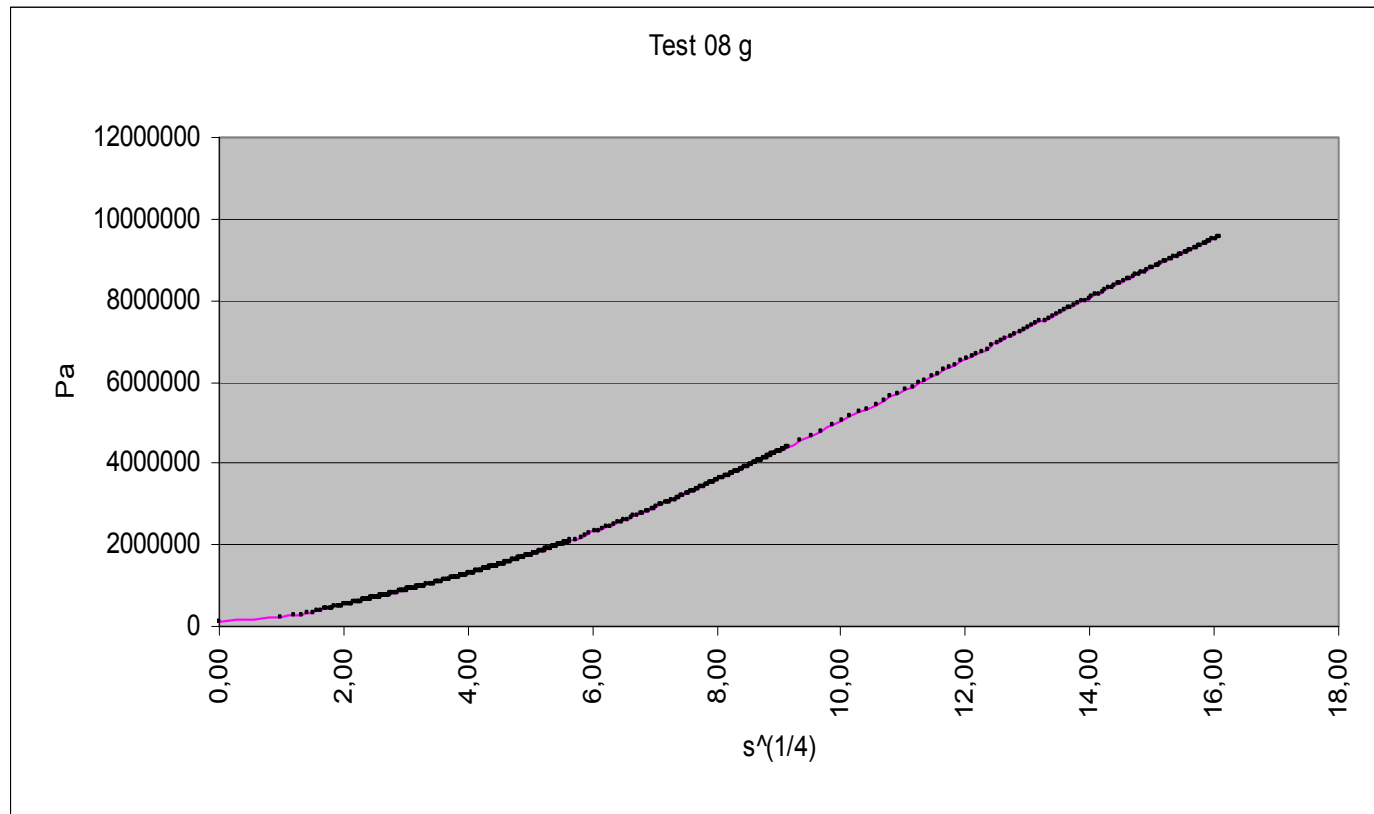


$$T_D = 1$$

post frac tests



post frac tests



$$T_D = 10$$

