Casing Design for Extreme Temperature



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Basic assumptions

- The hole will be cased off down to the critical point
- Bottom Hole Temperature max 550 C
- Bottom Hole Pressure max 26,7 MPa
- ASME and ASA codes or standards has to be "intertwine" into API standards
- The well shall be "safe" in flowing and closed conditions

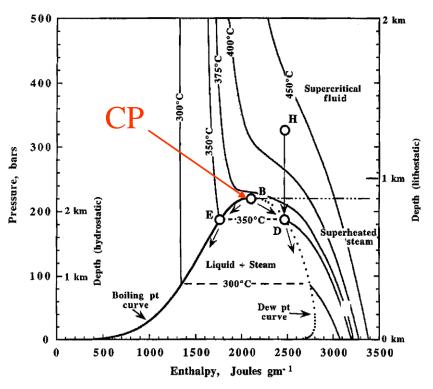


Critical Point (CP)

CP represents the highest temperature and pressure at which the substance can exist as a vapour and liquid in equilibrium.

CP for water: $T_{C} = 374 \ ^{\circ}C$

 $P_{C} = 22,1 \text{ MPa}$





Temperature and pressure assumptions above CP

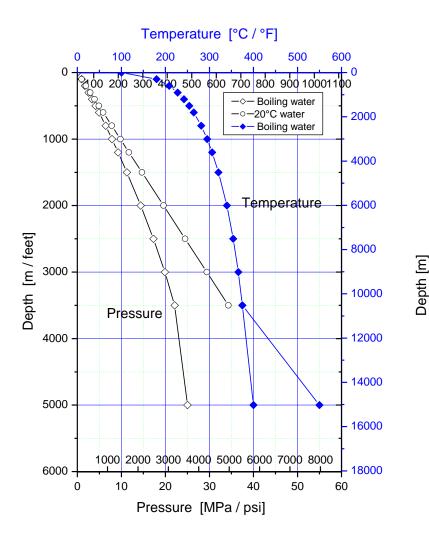
Boiling point curve to CP (3400 – 3500 m)
Hydrostatic conditions to CP

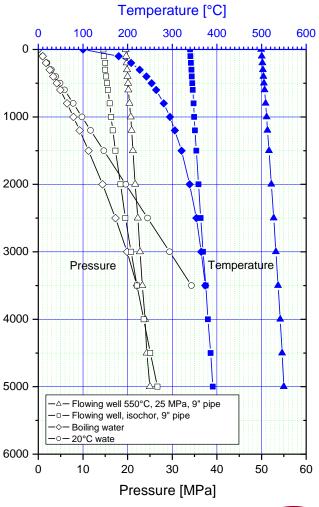
below CP

- Temperature will increase by 100 °C/km or
- Constant density with depth (Icochor)



Reservoir temperature and pressure Static and Flowing



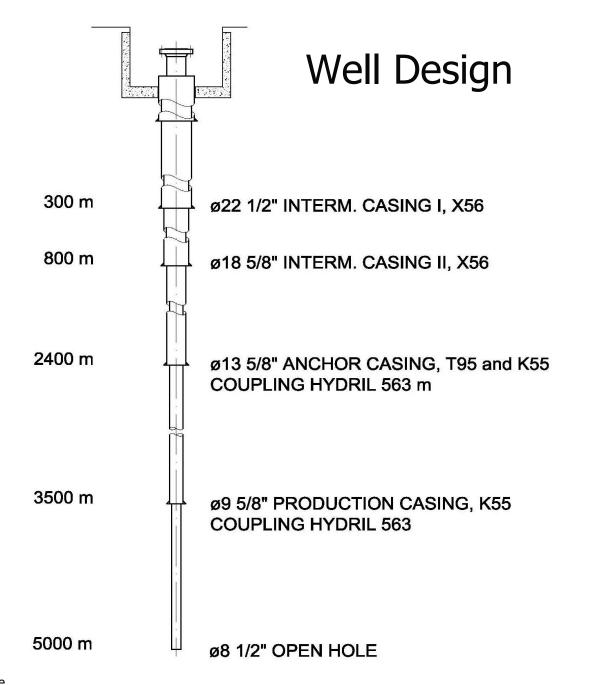




Design conditions

Basic parameters at wellhead Flowing well: ■T= 500°C and P= 19,5 MPa (Linear) ■T= 340°C and P= 14,5 MPa (Isochor) Closed well: ■T= 400°C and P= 22 MPa ■T= 20°C and P= 26.7 MPa







Conclusions

Diameter:

- ø13 5/8", 88,2 lbs/ft for top 300 m of anchor casing
- ø13 3/8", 72,0 lbs/ft for 300 to 2400 m of anchor casing
- Ø9 5/8", 53,5 lbs/ft production casing

Casing materials:

- T-95 type 1 and K-55 for anchor casing
- K-55 for production casing

Casing connections:

Hydril 563 (coupling and thread)

Wellhead flange:

ø10" ANSI, Class 2500 (material group 1.9, ANSI B16.5)

Wellhead master vale:

ø10" ANSI, Class 2500 (material group 1.9, ANSI B16.34)



Stress Calculations

axially σ_z ; tangentially σ_t ; radially σ_r

$$\sigma_z = \frac{P_m A_p}{A_r}, \qquad \sigma_t = \frac{P_m D_i}{2t}, \quad \sigma_r = -\frac{P_m}{2},$$

Internal overpressure P_m (MPa) Internal pipe area A_p , (mm²) Cross-sectional area of pipe wall A_r (mm²) Internal pipe diameter D_i (mm) Pipe wall thickness t (mm).



Stress Intensity

Permissible stress levels:

$$S_1 = |\sigma_z - \sigma_t|; S_2 = |\sigma_t - \sigma_r|; S_3 = |\sigma_r - \sigma_z|$$

stress intensity S $S = \max(S_1, S_2, S_3)$



Allowable Stress

$$S_m = \min\left[\frac{2}{3}S_Y, \frac{2}{3}S_YR_Y, \frac{1}{3}S_T, \frac{1}{3}S_TR_T\right]$$

SY = minimum yield strength at room temperature

ST = minimum tensile strength at room temperature

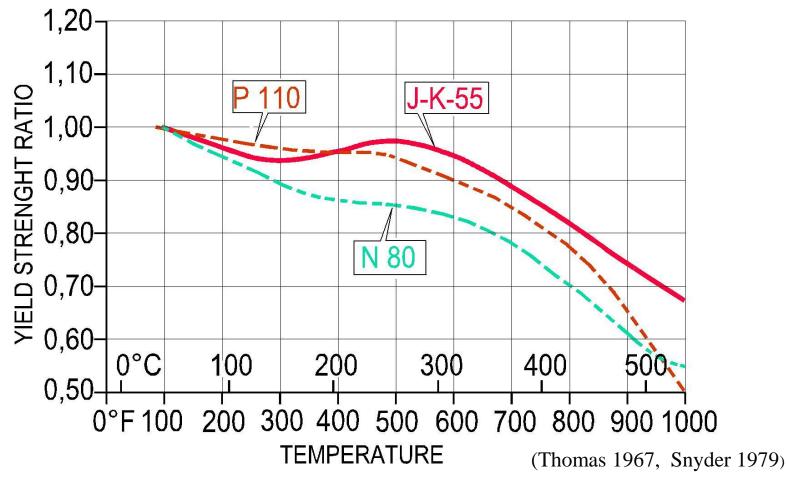
RY and RT are the ratios of minimum yield strength and minimum tensile strength at working temperature to room temperature respectively.

Stress Intensity < Allowable Stress

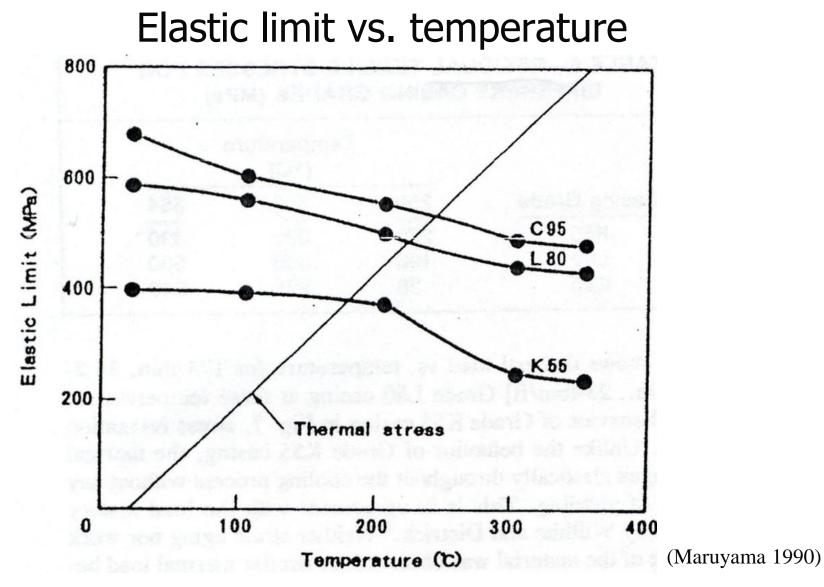
 $S < S_m$



Casing material at elevated temperature

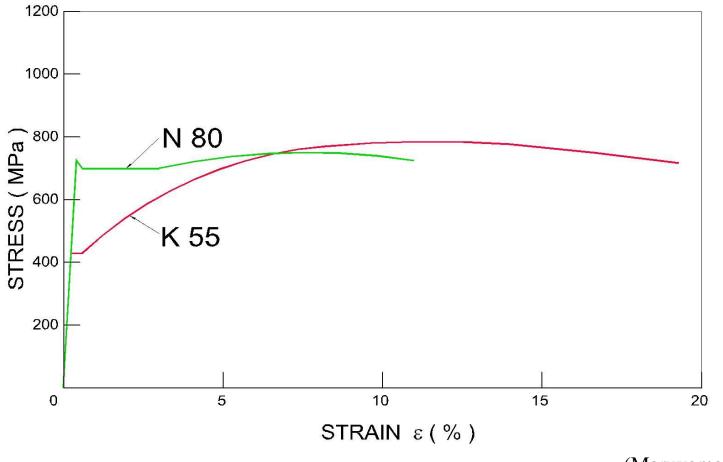








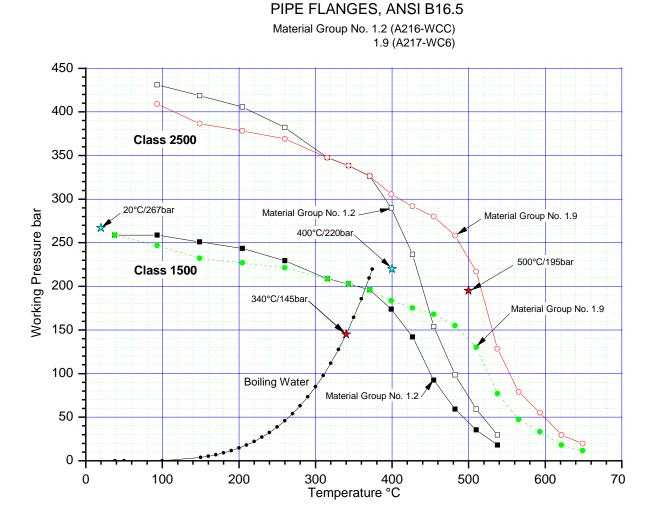
Tensile stress/strain curves



(Maruyama 1990)



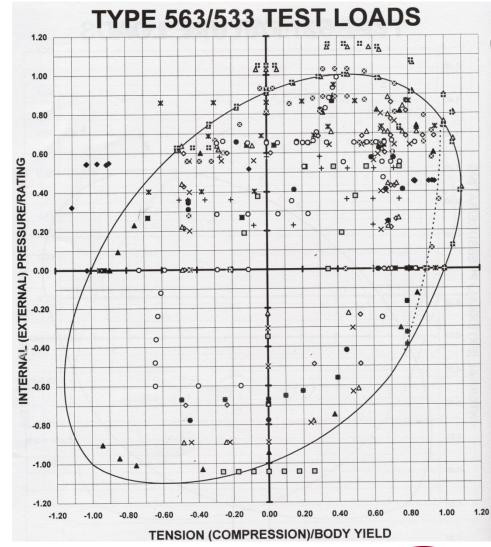
ANSI B16.34 Wellhead master valve selection criteria





HYDRIL connections, type 563







Final Points

- Information on casing material at temperature higher than 350 C are scarce
- K55 appears to be the best suitable material
- Creep resistant material is needed for top part of anchor casing API T95
- Premium connection are essential HYDRIL
 563
- Stress relaxation for K55 and L80 can be expected for temperature as low as 250 C
- Thermal cycling should be kept to minimum





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July 3, 2007: Engine